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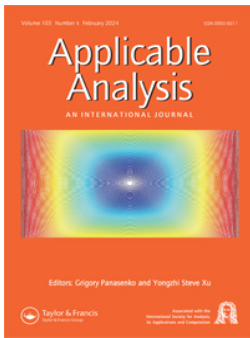
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Exact solutions for geophysical flows with discontinuous variable density and forcing terms in spherical coordinates

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ABSTRACT

We present here exact solutions to the equations of geophysical fluid dynamics that depict inviscid flows moving in the azimuthal direction on a circular path, around the globe, and which admit a velocity profile below the surface and along it. These features render this model suitable for the description of the Antarctic circumpolar current (ACC). The governing equations we work with—taken to be the Euler equations written in spherical coordinates—also incorporate forcing terms which are generally regarded as means that ensure the general balance of the ACC. Our approach allows for a variable density (depending on the depth and latitude) of discontinuous type which divides the water domain into two layers. Thus, the discontinuity gives rise to an interface. The velocity in both layers and the pressure in the lower layer are determined explicitly, while the pressure in the upper layer depends on the free surface and the interface. Functional analytical techniques render (uniquely) the surface and interface-defining functions in an implicit way. We conclude our discussion by deriving relations between the monotonicity of the surface pressure and the monotonicity of the surface distortion that concur with the physical expectations. A regularity result concerning the interface is also derived.

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1. Introduction

We present here a mathematical perspective concerning geophysical water flows exhibiting stratification, internal waves and a preferred (azimuthal) propagation direction. This task is carried out by deriving and analysing a family of exact solutions to the geophysical water wave equations written in spherical coordinates, in a rotating coordinate frame with the origin at a point on the Earth's surface that moves with the Earth and which incorporates forcing terms. These solutions describe incompressible, inviscid, stratified, steady flows moving on a circular path in the azimuthal direction completely around the globe and possessing a velocity profile below the surface and along it.

The previously mentioned aspects greatly apply to the Antarctic circumpolar current (Antarctic circumpolar current)—the only major current that circumnavigates the globe flowing eastwards through the southern regions of the Atlantic, Indian and Pacific Oceans along 23,000 km and having (in places) a width of over 2000 km, cf. Refs. [1–4]. More precisely, the earlier mentioned forcing terms provide the dynamical balance of ACC, cf. Refs. [5,6].

An important feature of geophysical flows, also discussed here, is stratification. Indeed, it is known [7,8] that in the southern oceans, strong meridional changes in air-sea buoyancy flux give rise to a strong polar front along which the ACC flows in thermal wind balance with the density gradients. One way in which stratification emerges is through eddies: it is argued in Ref. [7] that in collusion with imposed patterns of mechanical and buoyancy forcing, the eddies can set the stratification in both horizontal and vertical directions. Stratification also accommodates observed sharp changes in water density (due to variations in temperature and salinity, cf. Refs. [9–13]), known as *fronts* or *jets*, cf. Ref. [14].

In regard to the aspects mentioned earlier, we consider here a discontinuous density stratification of general type: mindful of the earlier described stratification induced by eddies, we allow the density to vary in the horizontal and vertical directions. Thus, in terms of spherical coordinates, the density that we consider here varies in the radial and latitudinal coordinates, respectively.

Although complicated analytical issues concerning stratification were dealt with in the case of two-dimensional flows, cf. Refs. [9,15–27], progress on the important issue of stratification in geophysical flows materialized only relatively recently, after the important developments by Constantin and Johnson [5,28] who constructed by means of spherical coordinates exact solutions to the geophysical fluid dynamics (GFD) equations representing azimuthal, depth-varying flows of constant density, which were able to capture the salient features of the equatorial undercurrent (EUC) and ACC, respectively. For a selective list of recent works concerning exact solutions in GFD, we refer to Refs. [5,9,10,28–40]. Building upon the approaches in Refs. [5,28], Henry and Martin [41–43] constructed exact solutions to GFD representing equatorial flows with continuously varying density depending on depth and latitude. This type of approach was extended to include discontinuous density, cf. Ref. [38], and discontinuously varying density together with forcing terms, cf. Refs. [44,45]. Here, we extend previous approaches [5,44,46–49] (regarding exact solutions pertaining to EUC and ACC) and so include forcing terms in the presence of a density stratification that varies (discontinuously) with respect to depth and latitude: we allow a vertical layering of the flow, with two layers of different, non-constant densities, where the denser layer sits below the less dense one (stable stratification). The discontinuity in density gives rise to an interface that behaves like an internal wave [7,8,18–20,50,51].

The layout of the paper is as follows: we introduce in Section 2 the governing equations (in spherical coordinates) and their boundary conditions for geophysical flows. Thereafter, we derive in Section 3 explicit solutions for the velocity field and the corresponding pressure function in the two layers of the fluid domain. From the dynamic boundary condition, we find an implicit relation between the imposed pressure and the resulting surface distortion. The interface defining function appears also implicitly as a condition expressing the balance of forces at the interface. In conjunction with the implicit function theorem, the two implicit equations are used to prove that any small enough perturbation of the pressure required to preserve an undisturbed free surface (following the curvature of the Earth) triggers unique functions, describing the surface and the interface, respectively. Finally, we prove that the solution we derived displays expected physical properties: a decay of the surface height occurs as soon as the pressure along the free surface increases. Moreover, we also prove that the interface defining function has very good regularity properties.

2. Physical problem and governing equations

In this section, we provide the governing equations for geophysical flows written in spherical coordinates to accommodate the shape of the Earth, together with the boundary conditions for the free surface and a rigid bed.

We will work in a system of right handed coordinates (r, θ, φ) where r denotes the distance to the centre of the sphere, $\theta \in [0, \pi]$ is the polar angle (the convention being that $\pi/2 - \theta$ is the angle of latitude) and $\varphi \in [0, 2\pi]$ is the azimuthal angle (the angle of longitude). While in this coordinate system the North and South poles are located at $\theta = 0, \pi$, respectively, the Equator sits on $\theta = \pi/2$,

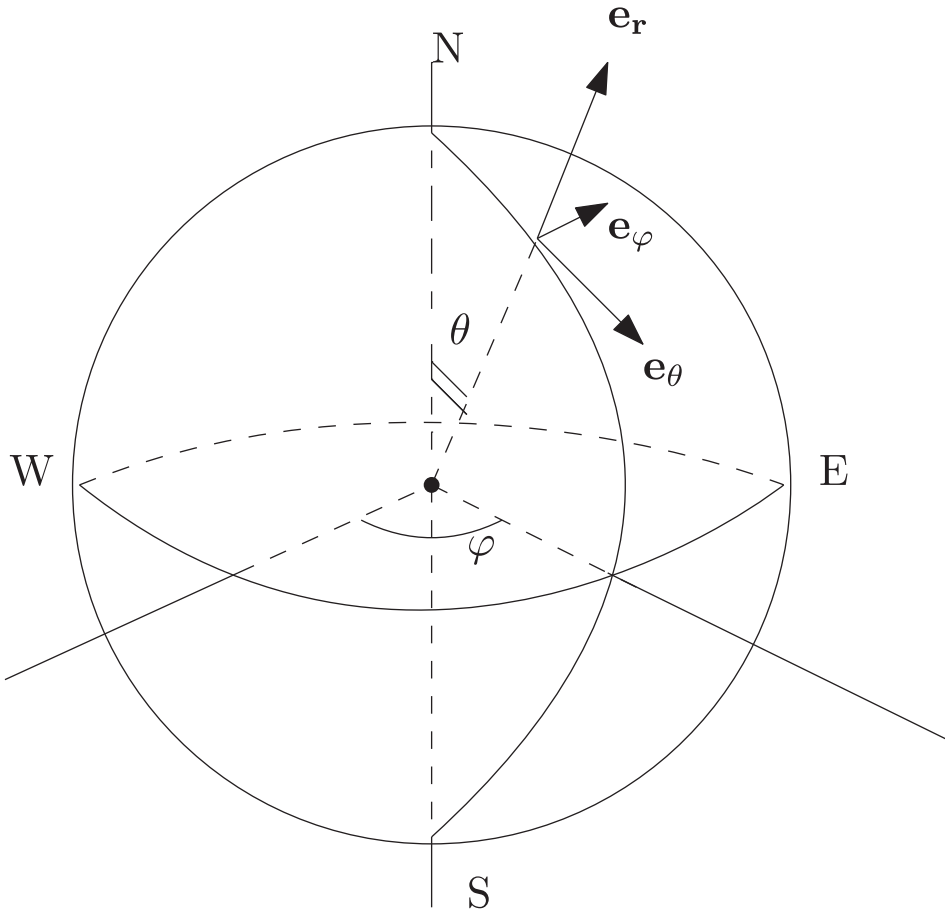


Figure 1. The spherical coordinate system: θ is the polar angle, φ is the azimuthal angle (the angle of longitude) and r represents the distance to the origin.

and the ACC is situated at $\theta = 3\pi/4$. The unit vectors in this system are

$$\begin{aligned} \mathbf{e}_r &= (\sin \theta \cos \varphi, \sin \theta \sin \varphi, \cos \theta), \\ \mathbf{e}_\theta &= (\cos \theta \cos \varphi, \cos \theta \sin \varphi, -\sin \theta), \\ \mathbf{e}_\varphi &= (-\sin \varphi, \cos \varphi, 0) \end{aligned}$$

with \mathbf{e}_φ pointing from West to East and \mathbf{e}_θ from North to South, cf. Figure 1.

Throughout this paper, we make the following simplifying assumption on the location of the ACC. We assume that the angle of latitude θ lies in the compact interval I_θ :

$$\theta \in I_\theta := \left[\frac{3\pi}{4} - \frac{\pi}{18}, \frac{3\pi}{4} + \frac{\pi}{18} \right]. \tag{1}$$

We are guided in our study by the observations made in Ref. [52] asserting that the Reynolds number is, in general, extremely large for oceanic flows. Accordingly, we will consider incompressible and inviscid flows. For $0 < r_2 < r_1 \ll R$ and $R_j := R + r_j$, $j = 1, 2$, we consider the two fluid layers D_j separated by an interface and bounded by the bottom and a free surface, which are described by the graphs of the functions h , d and k , respectively:

$$D_1 := \{(r, \theta, \varphi) : R_2 + h(\theta, \varphi) \leq r \leq R_1 + k(\theta, \varphi)\},$$

$$D_2 := \{(r, \theta, \varphi) : R + d(\theta, \varphi) \leq r \leq R_2 + h(\theta, \varphi)\}.$$

We associate R with the Earth's radius. The given function d describes the bottom topography, whereas h and k describe the unknown deviations of the interface and the free surface from their unperturbed locations at R_2 and R_1 , respectively. In particular, the density, ρ , is discontinuous with a jump at the interface $R_2 + h$. More precisely, $\rho = \rho_1(r, \theta)$ in D_1 and $\rho = \rho_2(r, \theta)$ in D_2 .

Let

$$\mathbf{u} = w\mathbf{e}_r + v\mathbf{e}_\theta + u\mathbf{e}_\varphi.$$

Then the Euler equations in the rotating frame for (w_j, v_j, u_j) within D_j , $j = 1, 2$, are given by

$$\begin{aligned} w_{j,t} + w_j w_{j,r} + \frac{v_j}{r} w_{j,\theta} + \frac{u_j}{r \sin \theta} w_{j,\varphi} - \frac{1}{r} (v_j^2 + u_j^2) - 2\Omega u_j \sin \theta - r\Omega^2 \sin^2 \theta \\ = -\frac{p_{j,r}}{\rho} + \mathfrak{F}_j^r, \\ v_{j,t} + w_j v_{j,r} + \frac{v_j}{r} v_{j,\theta} + \frac{u_j}{r \sin \theta} v_{j,\varphi} + \frac{1}{r} (w_j v_j - u_j^2 \cot \theta) - 2\Omega u_j \cos \theta - r\Omega^2 \sin \theta \cos \theta \\ = -\frac{p_{j,\theta}}{r\rho} + \mathfrak{F}_j^\theta, \\ u_{j,t} + w_j u_{j,r} + \frac{v_j}{r} u_{j,\theta} + \frac{u_j}{r \sin \theta} u_{j,\varphi} + \frac{1}{r} (w_j u_j + v_j u_j \cot \theta) + 2\Omega w_j \sin \theta + 2\Omega v_j \cos \theta \\ = -\frac{p_{j,\varphi}}{r\rho \sin \theta} + \mathfrak{F}_j^\varphi, \end{aligned} \quad (2)$$

which incorporate both Coriolis effects and centripetal acceleration ($\Omega \approx 7.29 \times 10^{-5} \text{ rad s}^{-1}$ refers to the constant rotation speed of the Earth), cf. Ref. [28]. Here, $p_j(r, \theta, \varphi)$ denotes the pressure field and $\mathfrak{F}_j = (\mathfrak{F}_j^r \mathbf{e}_r, \mathfrak{F}_j^\theta \mathbf{e}_\theta, \mathfrak{F}_j^\varphi \mathbf{e}_\varphi)$ is the body-force vector. Additionally to (2), the equation of mass conservation is required to be satisfied:

$$\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \rho w_j) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\rho v_j \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \varphi} (\rho u_j) = 0. \quad (3)$$

The GFD (2) and (3) are supplemented with the following boundary conditions. At the free surface $r = R_1 + k(\theta, \varphi)$, we require the dynamic boundary condition

$$p_1 = P_1(\theta, \varphi) \quad (4)$$

(for a prescribed function P_1) and the kinematic boundary condition

$$w_1 = \frac{v_1}{r} \frac{\partial k}{\partial \theta} + \frac{u_1}{r \sin \theta} \frac{\partial k}{\partial \varphi} \quad (5)$$

to be satisfied. At the interface $r = R_2 + h(\theta, \varphi)$, we require the normal components of the velocity fields \mathbf{u}_j to be equal:

$$\begin{aligned} (w_1 \mathbf{e}_r + v_1 \mathbf{e}_\theta + u_1 \mathbf{e}_\varphi) \cdot \left(\mathbf{e}_r - \frac{h_\theta}{r} \mathbf{e}_\theta - \frac{h_\varphi}{r \sin \theta} \mathbf{e}_\varphi \right) \\ = (w_2 \mathbf{e}_r + v_2 \mathbf{e}_\theta + u_2 \mathbf{e}_\varphi) \cdot \left(\mathbf{e}_r - \frac{h_\theta}{r} \mathbf{e}_\theta - \frac{h_\varphi}{r \sin \theta} \mathbf{e}_\varphi \right). \end{aligned} \quad (6)$$

Moreover, to ensure the balance of forces, we require that

$$p_1 = p_2 \quad \text{on} \quad R_2 + h(\theta, \varphi). \tag{7}$$

At the rigid ocean bottom $r = d(\theta, \varphi)$, it holds that

$$w_2 = \frac{v_2}{r} \frac{\partial d}{\partial \theta} + \frac{u_2}{r \sin \theta} \frac{\partial d}{\partial \varphi}. \tag{8}$$

3. Exact solutions

This section is concerned with the derivation of exact solutions to the problem (2)–(8). We first establish explicit formulas for the velocity field and the pressure in the layers D_1 and D_2 . Subsequently, we prove an existence type result for the surface and interface defining functions, respectively, by exploiting the balance of forces at the interface between the two fluid domains D_1 and D_2 .

3.1. The velocity field and the pressure

We seek a steady flow governed by (2) with $\mathfrak{F}_j(r, \theta) := (-g, G(r, \theta), 0)$, where g is the gravity of Earth and G denotes a general body force vector in θ direction, and (3) together with (4)–(8), which propagates purely in the azimuthal direction and does not depend on φ . Therefore, the velocity field satisfies $w_j = v_j = 0$ and $u_j = u_j(r, \theta)$, $p_j = p_j(r, \theta)$, $h = h(\theta)$, $k = k(\theta)$, and for consistency $d = d(\theta)$. Without loss of generality, we will assume that

$$h\left(\frac{3\pi}{4}\right) = 0. \tag{9}$$

Then (3) and (4)–(8) are automatically satisfied, while the Euler equations reduce to

$$\begin{cases} -\frac{u_j^2}{r} - 2\Omega u_j \sin \theta - r\Omega^2 \sin^2 \theta = -\frac{p_{j,r}}{\rho} - g, \\ -\frac{u_j^2}{r} \cot \theta - 2\Omega u_j \cos \theta - r\Omega^2 \sin \theta \cos \theta = -\frac{p_{j,\theta}}{\rho r} + G(r, \theta), \\ 0 = p_{j,\varphi}. \end{cases} \tag{10}$$

Remark 3.1: Concerning the nature of the forcing term above, it is argued in Ref. [5] that a relevant choice is

$$G(r, \theta) = -2\Omega u_0 \cos \theta, \tag{11}$$

where u_0 is the velocity of a linear flow which comes about by ignoring the nonlinear advection terms in (10).

We remark that the system (10) can be written as

$$\begin{cases} \rho \frac{(u_j + \Omega r \sin \theta)^2}{r} = p_{j,r} + g\rho, \\ \rho(u_j + \Omega r \sin \theta)^2 \cot \theta = p_{j,\theta} - \rho r G(r, \theta). \end{cases} \tag{12}$$

The shape of the previous system calls for the elimination of the pressure. Indeed, denoting

$$U_j(r, \theta) := \frac{(u_j + \Omega r \sin \theta)^2}{r}$$

for $j = 1, 2$, we obtain that U_j satisfies

$$\sin \theta \frac{\partial(\rho(r, \theta)rU_j)}{\partial \theta} - r \cos \theta \frac{\partial(\rho(r, \theta)rU_j)}{\partial r} = r \sin \theta \left(g\rho_\theta + \frac{\partial(\rho rG)}{\partial r} \right) \tag{13}$$

in $D_j, j = 1, 2$. Utilizing the method of characteristics (cf. Ref. [42]), we infer from the previous equation that the azimuthal velocity $u_j (j = 1, 2)$ is given as

$$u_j(r, \theta) = -\Omega r \sin \theta + \sqrt{\frac{F_j(r \sin \theta) + r \sin \theta \int_0^{f(\theta)} [H_{j,r}(\bar{r}(s), \bar{\theta}(s)) + g\rho_{j,\theta}(\bar{r}(s), \bar{\theta}(s))] ds}{\rho_j(r, \theta)}} \tag{14}$$

for some arbitrary continuously differentiable functions $x \mapsto F_j(x), j = 1, 2$, differentiable functions and

$$f(\theta) := \frac{1}{2} \ln \frac{1 - \cos \theta}{1 + \cos \theta}, \quad H_j(r, \theta) := r\rho_j(r, \theta)G(r, \theta)|_{r \in D_j},$$

$$\bar{r}(s) := r \sin \theta \cosh(s), \quad \bar{\theta}(s) := \arccos(-\sinh(s)). \tag{15}$$

Plugging (14) into (12) yields that

$$p_{j,r} = -g\rho_j(r, \theta) + \frac{F_j(r \sin \theta)}{r} + \sin \theta \int_0^{f(\theta)} [H_{j,r}(\bar{r}(s), \bar{\theta}(s)) + g\rho_{j,\theta}(\bar{r}(s), \bar{\theta}(s))] ds, \tag{16a}$$

$$p_{j,\theta} = H_j(r, \theta) + \cot \theta \left(F_j(r \sin \theta) + r \sin \theta \int_0^{f(\theta)} [H_{j,r}(\bar{r}(s), \bar{\theta}(s)) + g\rho_{j,\theta}(\bar{r}(s), \bar{\theta}(s))] ds \right). \tag{16b}$$

Introducing the change of variables $y = r \sin \theta$ and integrating (16a) for $r \in [R + d(\theta), R_2 + h(\theta)]$ leads to

$$p_2(r, \theta) = -g \int_{R+d(\theta)}^r \rho_2(r', \theta) dr' + \int_{(R+d(\theta)) \sin \theta}^{r \sin \theta} \left[\frac{F_2(y)}{y} + \mathcal{F}_2(y, \theta) \right] dy + C_2(\theta), \tag{17}$$

where $\theta \rightarrow C_2(\theta)$ is a function such that

$$C_2'(\theta) = H_2(R + d(\theta), \theta) - g\rho_2(R + d(\theta), \theta)d'(\theta) + \left[\frac{F_2((R + d(\theta)) \sin \theta)}{(R + d(\theta)) \sin \theta} + \mathcal{F}_2((R + d(\theta)) \sin \theta, \theta) \right] ((R + d(\theta)) \sin \theta)'$$

$$\tag{18}$$

and

$$\mathcal{F}_j(y, \theta) := \int_0^{f(\theta)} [H_{j,r}(y \cosh(s), \bar{\theta}(s)) + g\rho_{j,\theta}(y \cosh(s), \bar{\theta}(s))] ds \quad \text{for } j = 1, 2.$$

Denoting $\mathcal{F}_{j,\theta}(y, \theta) := (\partial \mathcal{F}_j / \partial \theta)(y, \theta)$, we have from the above that

$$\mathcal{F}_{j,\theta}(y, \theta) = \csc \theta [H_{j,r}(y \csc \theta, \theta) + g\rho_{j,\theta}(y \csc \theta, \theta)], \quad j = 1, 2, \tag{19}$$

which will be used later.

Following the same procedure for $p_1(h, r, \theta)$ and using (9), we get:

$$p_1(h, r, \theta) = -g \int_{R_2+h(\theta)}^r \rho_1(\tilde{r}, \theta) d\tilde{r} + \int_{(R_2+h(\theta)) \sin \theta}^{r \sin \theta} \left[\frac{F_1(y)}{y} + \mathcal{F}_1(y, \theta) \right] dy + C_1(h, \theta), \quad (20)$$

where

$$\begin{aligned} C_1(h, \theta) = & \int_{3\pi/4}^{\theta} H_1(R_2 + h(\tilde{\theta}), \tilde{\theta}) d\tilde{\theta} - g \int_{3\pi/4}^{\theta} \rho_1(R_2 + h(\tilde{\theta}), \tilde{\theta}) h'(\tilde{\theta}) d\tilde{\theta} \\ & + \int_{3\pi/4}^{\theta} \left[\frac{F_1((R_2 + h(\tilde{\theta})) \sin \tilde{\theta})}{(R_2 + h(\tilde{\theta})) \sin \tilde{\theta}} + \mathcal{F}_1((R_2 + h(\tilde{\theta})) \sin \tilde{\theta}, \tilde{\theta}) \right] ((R_2 + h(\tilde{\theta})) \sin \tilde{\theta})' d\tilde{\theta} + c \end{aligned} \quad (21)$$

for some constant c .

3.2. Implicit equations for the free surface and for the interface

This section is devoted to the determination of the free surface and of the interface. To begin with, we exploit now the balance of forces at the interface $r = R_2 + h(\theta)$ in order to obtain an equation for the function $\theta \rightarrow h(\theta)$. That is, Equation (7) reads now

$$p_1(R_2 + h(\theta), \theta) = p_2(R_2 + h(\theta), \theta), \quad (22)$$

which can be written equivalently as

$$C_1(h, \theta) = \int_{(R_2+h(\theta)) \sin \theta}^{(R_2+h(\theta)) \sin \theta} \left(\frac{F_2(y)}{y} + \mathcal{F}_2(y, \theta) \right) dy - g \int_{R_2+h(\theta)}^{R_2+h(\theta)} \rho_2(\tilde{r}, \theta) d\tilde{r} + C_2(\theta). \quad (23)$$

We now pass to a functional analytic setting and so we define nondimensional quantities. First, we set

$$\langle(\theta) := \frac{h(\theta)}{R_2}, \quad \parallel(\theta) := \frac{k(\theta)}{R_1}.$$

We can now write (23) as

$$\mathcal{G}_2(\langle) = 0, \quad (24)$$

where the operator \mathcal{G}_2 acts from the Banach space $C^1(I_\theta)$ into itself and is given as

$$\begin{aligned} \mathcal{G}_2(\langle)(\theta) := & \frac{1}{P_{\text{atm}}} \left(\int_{(R_2+h(\theta)) \sin \theta}^{(1+\langle(\theta))R_2 \sin \theta} \left(\frac{F_2(y)}{y} + \mathcal{F}_2(y, \theta) \right) dy - g \int_{R_2+h(\theta)}^{(1+\langle(\theta))R_2} \rho_2(\tilde{r}, \theta) d\tilde{r} \right) \\ & - \frac{C_1(\langle, \theta) + C_2(\theta)}{P_{\text{atm}}}, \end{aligned} \quad (25)$$

where P_{atm} denotes the constant atmospheric pressure.

To obtain an equation for the free surface (non-dimensional) defining function, we utilize the dynamic condition at the surface (4), and so obtain the equation

$$P_1(\theta) = -g \int_{R_2+h(\theta)}^{R_1+k(\theta)} \rho_1(\tilde{r}, \theta) d\tilde{r} + \int_{(R_2+h(\theta)) \sin \theta}^{(R_1+k(\theta)) \sin \theta} \left[\frac{F_1(y)}{y} + \mathcal{F}_1(y, \theta) \right] dy + C_1(h, \theta), \quad (26)$$

called the Bernoulli relation. The latter provides a connection between the pressure at the free surface and the shape of the free surface and of the interface, respectively. Setting $\mathcal{P}_1(\theta) := P_1(\theta)/P_{\text{atm}}$, we

can rewrite the Bernoulli relation as the operator equation

$$\mathcal{G}_1(\|\cdot\|, \langle \cdot \rangle, \mathcal{P}_1) = 0, \tag{27}$$

where \mathcal{G}_1 is an operator from the Banach space $C(I_\theta) \times C^1(I_\theta) \times C(I_\theta)$ into itself and is given through

$$\begin{aligned} \mathcal{G}_1(\|\cdot\|, \langle \cdot \rangle, \mathcal{P}_1)(\theta) &:= \\ &= \frac{1}{P_{\text{atm}}} \left(\int_{(1+\langle(\theta)\rangle)R_2 \sin \theta}^{(1+\|\theta\|)R_1 \sin \theta} \left(\frac{F_1(y)}{y} + \mathcal{F}_1(y, \theta) \right) dy - g \int_{(1+\langle(\theta)\rangle)R_2}^{(1+\|\theta\|)R_1} \rho_1(\tilde{r}, \theta) d\tilde{r} + C_1(\langle \cdot \rangle, \theta) \right) \\ &\quad - \mathcal{P}_1(\theta). \end{aligned} \tag{28}$$

Remark 3.2: The previous discussion shows now that the unknowns $(\|\cdot\|, \langle \cdot \rangle)$ are solutions to the equation

$$(\mathcal{G}_1(\|\cdot\|, \langle \cdot \rangle, \mathcal{P}_1), \mathcal{G}_2(\langle \cdot \rangle)) = 0, \tag{29}$$

which will be studied by availing of the implicit function theorem [53]. To this end, we identify first a pair $(\|\cdot\|, \langle \cdot \rangle)$ of explicit solutions to (29).

Denoting by P_1^0 the surface pressure for the undisturbed interface ($h(\theta) = 0$) and free surface ($k(\theta) = 0$), we derive from (26) that

$$\begin{aligned} P_1^0(\theta) &= -g \int_{R_2}^{R_1} \rho_1(\tilde{r}, \theta) d\tilde{r} + \int_{R_2 \sin \theta}^{R_1 \sin \theta} \left[\frac{F_1(y)}{y} + \mathcal{F}_1(y, \theta) \right] dy \\ &\quad + \int_{3\pi/4}^{\theta} \left[F_1(R_2 \sin \tilde{\theta}) \cot \tilde{\theta} + \mathcal{F}_1(R_2 \sin \tilde{\theta}, \tilde{\theta}) R_2 \cos \tilde{\theta} + H_1(R_2, \tilde{\theta}) \right] d\tilde{\theta}. \end{aligned} \tag{30}$$

Setting now $\mathcal{P}_1^0(\theta) = P_1^0/P_{\text{atm}}$ and $\langle \cdot \rangle_0 := 0, \|\cdot\|_0 := 0$, we have from (28) and (30) that

$$\mathcal{G}_1(\|\cdot\|_0, \langle \cdot \rangle_0, \mathcal{P}_1^0) = 0.$$

Furthermore, $\mathcal{G}_2(\langle \cdot \rangle_0) = 0$ if and only if

$$\int_{(R+d(\theta)) \sin \theta}^{R_2 \sin \theta} \left(\frac{F_2(y)}{y} + \mathcal{F}_2(y, \theta) \right) dy - g \int_{R+d(\theta)}^{R_2} \rho_2(\tilde{r}, \theta) d\tilde{r} - C_1(0, \theta) + C_2(\theta) = 0. \tag{31}$$

To be able to apply the implicit function theorem to Equation (29), we need to compute the derivatives of the operator involved in (29). First, we compute $(\mathcal{G}_{2, \langle \cdot \rangle}(\langle \cdot \rangle)(\theta) = \lim_{s \rightarrow 0} (\mathcal{G}_2(s \langle \cdot \rangle)(\theta) - \mathcal{G}_2(0)(\theta))/s$. We obtain

$$\begin{aligned} (\mathcal{G}_{2, \langle \cdot \rangle}(\langle \cdot \rangle)(\theta)) &= \frac{(F_2(R_2 \sin \theta) + (R_2 \sin \theta) \mathcal{F}_2(R_2 \sin \theta, \theta) - gR_2 \rho_2(R_2, \theta)) \langle \cdot \rangle(\theta)}{P_{\text{atm}}} \\ &\quad - \frac{C_{1, \langle \cdot \rangle}(\langle \cdot \rangle)(\theta)}{P_{\text{atm}}}. \end{aligned} \tag{32}$$

The fact that $h(3\pi/4) = 0$ and (19) yield

$$\begin{aligned} C_{1, \langle \cdot \rangle}(\langle \cdot \rangle)(\theta) &= R_2 \int_{3\pi/4}^{\theta} H_{1,r}(R_2, \tilde{\theta}) \langle \cdot \rangle(\tilde{\theta}) d\tilde{\theta} - gR_2 \rho_1(R_2, \theta) \langle \cdot \rangle(\theta) \\ &\quad + gR_2 \int_{3\pi/4}^{\theta} \rho_{1,\theta}(R_2, \tilde{\theta}) \langle \cdot \rangle(\tilde{\theta}) d\tilde{\theta} + (R_2 \sin \theta) \mathcal{F}_1(R_2 \sin \theta, \theta) \langle \cdot \rangle(\theta) \end{aligned}$$

$$\begin{aligned}
 & -R_2 \int_{3\pi/4}^{\theta} \mathcal{F}_{1,\theta}(R_2 \sin \tilde{\theta}, \tilde{\theta}) \langle \tilde{\theta} \rangle \sin \tilde{\theta} \, d\tilde{\theta} + F_1(R_2 \sin \theta) \langle \theta \rangle \\
 & = -gR_2 \rho_1(R_2, \theta) \langle \theta \rangle + (R_2 \sin \theta) \mathcal{F}_1(R_2 \sin \theta, \theta) \langle \theta \rangle \\
 & \quad + F_1(R_2 \sin \theta) \langle \theta \rangle.
 \end{aligned} \tag{33}$$

Thus,

$$\begin{aligned}
 & P_{\text{atm}}(\mathcal{G}_{2,\langle}(\mathbf{0}) \langle \cdot \rangle)(\theta) \\
 & = (F_2(R_2 \sin \theta) - F_1(R_2 \sin \theta) - gR_2(\rho_2(R_2, \theta) - \rho_1(R_2, \theta))) \langle \theta \rangle \\
 & \quad + (R_2 \sin \theta)(\mathcal{F}_2(R_2 \sin \theta, \theta) - \mathcal{F}_1(R_2 \sin \theta, \theta)) \langle \theta \rangle \\
 & = -gR_2(\rho_2(R_2, \theta) - \rho_1(R_2, \theta)) \langle \theta \rangle \\
 & \quad + (u_2(R_2, \theta) + \Omega R_2 \sin \theta)^2 \rho_2(R_2, \theta) \langle \theta \rangle \\
 & \quad - (u_1(R_2, \theta) + \Omega R_2 \sin \theta)^2 \rho_1(R_2, \theta) \langle \theta \rangle,
 \end{aligned} \tag{34}$$

where we have also used (14). Owing to the remark that the velocity in ocean flows does not exceed 1 m/s, we have that gR_2 clearly exceeds the quantity

$$(u_2(R_2, \theta) + \Omega R_2 \sin \theta)^2 \rho_2(R_2, \theta) - (u_1(R_2, \theta) + \Omega R_2 \sin \theta)^2 \rho_1(R_2, \theta).$$

Therefore, there exists a constant $\alpha < 0$ such that the inequality

$$\begin{aligned}
 & (u_2(R_2, \theta) + \Omega R_2 \sin \theta)^2 \rho_2(R_2, \theta) - (u_1(R_2, \theta) + \Omega R_2 \sin \theta)^2 \rho_1(R_2, \theta) \\
 & \quad - gR_2(\rho_2(R_2, \theta) - \rho_1(R_2, \theta)) \leq \alpha
 \end{aligned} \tag{35}$$

holds for all $\theta \in I_\theta$. This shows that $\mathcal{G}_{2,\langle}(\mathbf{0}) : C^1(I_\theta) \mapsto C^1(I_\theta)$ is a linear homeomorphism.

Clearly, $\mathcal{G}_{2,\|\|}(\mathbf{0})\| = 0$ for all $\|$.

$$\begin{aligned}
 P_{\text{atm}}(\mathcal{G}_{1,\|\|}(\mathbf{0}, \mathbf{0}, \mathcal{P}_1^0)\|)(\theta) & = R_1 \sin \theta \left(\frac{F_1(R_1 \sin \theta)}{R_1 \sin \theta} + \mathcal{F}_1(R_1 \sin \theta, \theta) \right) \|\|(\theta) \\
 & \quad - gR_1 \rho_1(R_1, \theta) \|\|(\theta) \\
 & = (u_1(R_1, \theta) + \Omega R_1 \sin \theta)^2 \rho_1(R_1, \theta) \\
 & \quad - gR_1 \rho_1(R_1, \theta) \|\|(\theta).
 \end{aligned} \tag{36}$$

Since the term gR_1 greatly outweighs the velocity term $(u_1(R_1, \theta) + \Omega R_1 \sin \theta)^2$, we can infer that there is a constant $\beta < 0$ such that

$$((u_1(R_1, \theta) + \Omega R_1 \sin \theta)^2 - gR_1) \rho_1(R_1, \theta) \leq \beta \quad \text{for all } \theta \in I_\theta. \tag{37}$$

The latter inequality allows us to conclude that the operator $\mathcal{G}_{1,\|\|}(\mathbf{0}, \mathbf{0}, \mathcal{P}_1^0) : C(I_\theta) \mapsto C(I_\theta)$ is a linear homeomorphism. Using now (28), we compute

$$\begin{aligned}
 (\mathcal{G}_{1,\langle}(\mathbf{0}, \mathbf{0}, \mathcal{P}_1^0) \langle \cdot \rangle)(\theta) & = \frac{-F_1(R_2 \sin \theta) - (R_2 \sin \theta) \mathcal{F}_1(R_2 \sin \theta, \theta) + gR_2 \rho_1(R_2, \theta)}{P_{\text{atm}}} \langle \theta \rangle \\
 & \quad + \frac{C_{1,\langle}(\mathbf{0}) \langle \cdot \rangle(\theta)}{P_{\text{atm}}} \\
 & = 0,
 \end{aligned} \tag{38}$$

the last equality being true by formula (33).

We can summarize the previous discussion by inserting the results into the matrix

$$\begin{aligned}
 (\mathcal{G}_1, \mathcal{G}_2)_{\|\cdot, \langle} (0, 0, \mathcal{P}_1^0) &= \begin{pmatrix} \mathcal{G}_{1,\|\cdot} (0, 0, \mathcal{P}_1^0) & \mathcal{G}_{1,\langle} (0, 0, \mathcal{P}_1^0) \\ \mathcal{G}_{2,\|\cdot} (0, 0, \mathcal{P}_1^0) & \mathcal{G}_{2,\langle} (0, 0, \mathcal{P}_1^0) \end{pmatrix} \\
 &= \begin{pmatrix} \mathcal{G}_{1,\|\cdot} (0, 0, \mathcal{P}_1^0) & 0 \\ 0 & \mathcal{G}_{2,\langle} (0, 0, \mathcal{P}_1^0) \end{pmatrix}, \tag{39}
 \end{aligned}$$

which is a linear operator $C(I_\theta) \times C^1(I_\theta) \mapsto C(I_\theta) \times C^1(I_\theta)$, that is also a homomorphism by the discussions following (35) and (37).

The previous considerations allow now the utilization of the implicit function theorem which guarantees the existence of a unique solution to Equation (29) representing the free surface and the interface of the flow with velocity field (14) and pressure given by (17) and (20). We formulate the result in the following theorem.

Theorem 3.3: *For any sufficiently small perturbation \mathcal{P}_1 of \mathcal{P}_1^0 , there is a unique $\langle \in C^1(I_\theta)$ solution to (24) and a unique $\|\in C(I_\theta)$ that satisfies (27).*

4. Properties of the exact solutions

This section is devoted to proving a regularity property of the interface as well as to deriving a relation between the monotonicity of the free surface and the monotonicity of the pressure exerted on the free surface.

Proposition 4.1: *Assuming that the azimuthal component of the velocity field does not exceed 1 ms^{-1} and that the change in density across the interface (represented by the function \langle) is at least 0.2 kg m^{-3} , we have that $\langle \in C^\infty(I_\theta)$, provided $\langle \in C^1(I_\theta)$ and the functions F_1, F_2 (giving the velocity fields in the two layers) are infinitely differentiable).*

Proof: We recall that, from Theorem 3.3, we have that $\langle \in C^1(I_\theta)$ satisfies $\mathcal{G}_2(\langle)(\theta) = 0$ for all $\theta \in I_\theta$. Passing to differentiation with respect to θ in the implicit equation for \langle , we have that

$$\begin{aligned}
 & (F_2 - F_1) \left((1 + \langle(\theta))R_2 \sin \theta \right) \frac{\langle'(\theta)}{1 + \langle(\theta)} \\
 & + (R_2 \sin \theta)(\mathcal{F}_2 - \mathcal{F}_1) \left((1 + \langle(\theta))R_2 \sin \theta, \theta \right) \langle'(\theta) \\
 & - gR_2(\rho_2 - \rho_1) \left((1 + \langle(\theta))R_2, \theta \right) \langle'(\theta) \\
 & + (F_2 - F_1) \left((1 + \langle(\theta))R_2 \sin \theta \right) \cot \theta \\
 & + (1 + \langle(\theta))R_2 \sin \theta (\mathcal{F}_2 - \mathcal{F}_1) \left((1 + \langle(\theta))R_2 \sin \theta, \theta \right) \cot \theta \\
 & + (H_2 - H_1) \left((1 + \langle(\theta))R_2, \theta \right) = 0. \tag{40}
 \end{aligned}$$

We aim to show in the following that the term from (40) multiplying $h'(\theta)$ has constant sign. To this end, we remark first that

$$\begin{aligned}
 & \frac{(F_2 - F_1) \left((1 + \langle(\theta))R_2 \sin \theta \right)}{1 + \langle(\theta)} + (R_2 \sin \theta)(\mathcal{F}_2 - \mathcal{F}_1) \left((1 + \langle(\theta))R_2 \sin \theta, \theta \right) \\
 & = \frac{\rho_1(R_2, \theta) \left[u_2^2 \left((1 + \langle(\theta))R_2, \theta \right) - u_1^2 \left((1 + \langle(\theta))R_2, \theta \right) \right]}{1 + \langle(\theta)}
 \end{aligned}$$

$$\begin{aligned}
 &+ 2\rho_1\Omega R_2(\sin\theta) [u_2((1 + \langle(\theta)\rangle)R_2, \theta) - u_1((1 + \langle(\theta)\rangle)R_2, \theta)] \\
 &+ \frac{(\rho_2 - \rho_1) [u_2((1 + \langle(\theta)\rangle)R_2, \theta) + \Omega R_2(1 + \langle(\theta)\rangle) \sin\theta]^2}{1 + \langle(\theta)\rangle} \\
 \leq &R_2 \left(\frac{\rho_1 u_2^2}{R_2} + 2\rho_1\Omega u_2 + \frac{(\rho_2 - \rho_1)(u_2 + \Omega R_2(1 + \langle(\theta)\rangle) \sin\theta)^2}{R_2} \right) \\
 < &gR_2(\rho_2 - \rho_1) ((1 + \langle(\theta)\rangle)R_2, \theta), \tag{41}
 \end{aligned}$$

where, in the last inequality, we have used the assumptions (about the ranges of the velocity field and of the differences in density across the interface, respectively) made in the statement of the proposition. Thus,

$$\begin{aligned}
 &\frac{(F_2 - F_1) ((1 + \langle(\theta)\rangle)R_2 \sin\theta)}{1 + \langle(\theta)\rangle} + (R_2 \sin\theta)(\mathcal{F}_2 - \mathcal{F}_1) ((1 + \langle(\theta)\rangle)R_2 \sin\theta, \theta) \\
 &- gR_2(\rho_2 - \rho_1) ((1 + \langle(\theta)\rangle)R_2, \theta) < 0, \tag{42}
 \end{aligned}$$

and so the assertion in the statement of the proposition is proved. ■

We conclude by some properties exhibited by the exact solutions derived earlier. These properties agree with what is observed on physical grounds and establish a connection between the free surface, $\|$, and the pressure \mathcal{P}_1 exerted on the surface. We will carry out the necessary arguments under the assumption that \mathcal{P}_1 is a differentiable function. A bootstrapping argument [53] ensures that the differentiability of \mathcal{P}_1 implies the differentiability of $\|$.

Theorem 4.2 (Monotonicity relations): *If the pressure \mathcal{P}_1 exerted on the free surface increases, then the surface itself must decrease. On the other hand, an amplification of the free surface can only happen in the presence of a decreasing pressure.*

Proof: We notice first that equality (19) entails

$$\begin{aligned}
 \int_{(1+\langle(\theta)\rangle)R_2 \sin\theta}^{(1+\|(\theta)\rangle)R_1 \sin\theta} \mathcal{F}_{1,\theta}(y, \theta) \, d\theta &= \int_{(1+\langle(\theta)\rangle)R_2}^{(1+\|(\theta)\rangle)R_1} (H_{1,r}(\xi, \theta) + g\rho_{1,\theta}(\xi, \theta)) \, d\xi \\
 &= H_1((1 + \|(\theta)\rangle)R_1, \theta) - H_1((1 + \langle(\theta)\rangle)R_2, \theta) \\
 &\quad + \int_{(1+\langle(\theta)\rangle)R_2}^{(1+\|(\theta)\rangle)R_1} g\rho_{1,\theta}(\xi, \theta) \, d\xi. \tag{43}
 \end{aligned}$$

Differentiating now in (27), we obtain by means of (43) that

$$\begin{aligned}
 &\mathcal{P}'_1(\theta)P_{\text{atm}} \\
 &= \left(\frac{F_1((1 + \|(\theta)\rangle)R_1 \sin\theta)}{1 + \|(\theta)\rangle} + R_1(\sin\theta)\mathcal{F}_1((1 + \|(\theta)\rangle)R_1 \sin\theta, \theta) \right) \|\prime(\theta) \\
 &+ (F_1((1 + \|(\theta)\rangle)R_1 \sin\theta) + (1 + \|(\theta)\rangle)R_1(\sin\theta)\mathcal{F}_1((1 + \|(\theta)\rangle)R_1 \sin\theta, \theta)) \cot\theta \\
 &+ \int_{(1+\langle(\theta)\rangle)R_2 \sin\theta}^{(1+\|(\theta)\rangle)R_1 \sin\theta} \mathcal{F}_{1,\theta}(y, \theta) \, d\theta \\
 &- gR_1\rho_1((1 + \|(\theta)\rangle)R_1, \theta) \|\prime(\theta) + gR_2\rho_1((1 + \langle(\theta)\rangle)R_1, \theta) \langle\prime(\theta)
 \end{aligned}$$

$$-g \int_{(1+\langle(\theta)\rangle)R_2}^{(1+\|(\theta)\rangle)R_1} \rho_{1,\theta}(\tilde{r}, \theta) d\tilde{r} + \frac{\partial}{\partial \theta} (C_1(h, \theta)). \quad (44)$$

Employing now (14), (21) and (43), we have

$$\begin{aligned} & \mathcal{P}'_1(\theta)P_{\text{atm}} \\ &= \left(\frac{(u_1((1+\|(\theta)\rangle)R_1 \sin \theta, \theta) + \Omega R_1(1+\|(\theta)\rangle \sin \theta))^2}{1+\|(\theta)\rangle} - gR_1 \right) \rho_1((1+\|(\theta)\rangle)R_1, \theta) \|\prime(\theta) \\ &+ (u_1((1+\|(\theta)\rangle)R_1 \sin \theta, \theta) + \Omega R_1(1+\|(\theta)\rangle \sin \theta))^2 \rho_1((1+\|(\theta)\rangle)R_1, \theta) \cot \theta \\ &+ (1+\|(\theta)\rangle)R_1 \rho_1((1+\|(\theta)\rangle)R_1, \theta) G((1+\|(\theta)\rangle)R_1, \theta). \end{aligned} \quad (45)$$

The proof of the enunciated property is concluded by noticing that the term

$$\begin{aligned} & (u_1((1+\|(\theta)\rangle)R_1 \sin \theta, \theta) + \Omega R_1(1+\|(\theta)\rangle \sin \theta))^2 \cot \theta \\ &+ (1+\|(\theta)\rangle)R_1 G((1+\|(\theta)\rangle)R_1, \theta) \end{aligned} \quad (46)$$

is negative. Indeed, replacing G from (11), the expression in (46) can be written as

$$\begin{aligned} & (u_1^2 + 2u_1\Omega R_1(1+\|(\theta)\rangle \sin \theta) \cot \theta \\ &+ \Omega R_1(1+\|(\theta)\rangle) (\Omega R_1(1+\|(\theta)\rangle \sin \theta - 2u_0) \cos \theta, \end{aligned} \quad (47)$$

where u_0 has the size of an azimuthal velocity. It is easy to see that the sizes of the physical quantities involved yield that the term $\Omega R_1(1+\|(\theta)\rangle \sin \theta)$ is much bigger than $2u_0$. This shows that the expression in (47) is negative for all $\theta \in I_\theta$. Furthermore, the realistic sizes of the quantities u_1 , Ω and R_1 yield that for all $\theta \in I_\theta$, it holds

$$\frac{(u_1((1+\|(\theta)\rangle)R_1 \sin \theta, \theta) + \Omega R_1(1+\|(\theta)\rangle \sin \theta))^2}{1+\|(\theta)\rangle} - gR_1 < 0. \quad (48)$$

These considerations show via (45) that if for some $\theta \in I_\theta$ holds that $\mathcal{P}'_1(\theta) \geq 0$, then we must have that $\|\prime(\theta) < 0$. Moreover, if there is $\theta \in I_\theta$ such that $\|\prime(\theta) \geq 0$, then, necessarily, it must hold that $\mathcal{P}'_1(\theta) < 0$. ■

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