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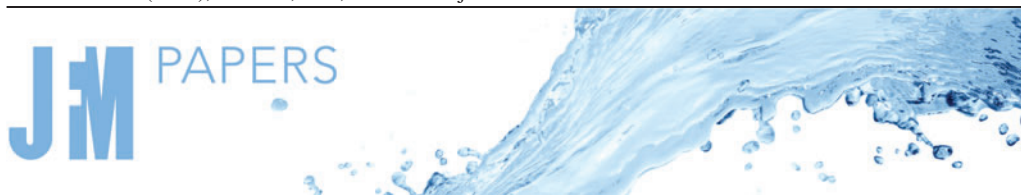
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Reynolds-number scaling of wall-pressure–velocity correlations in wall-bounded turbulence

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Wall-pressure fluctuations are a practically robust input for real-time control systems aimed at modifying wall-bounded turbulence. The scaling behaviour of the wall-pressure–velocity coupling requires investigation to properly design a controller with such input data so that it can actuate upon the desired turbulent structures. A comprehensive database from direct numerical simulations (DNS) of turbulent channel flow is used for this purpose, spanning a Reynolds-number range $Re_\tau \approx 550$ –5200. Spectral analysis reveals that the streamwise velocity is most strongly coupled to the linear term of the wall pressure, at a Reynolds-number invariant distance-from-the-wall scaling of $\lambda_x/y \approx 14$ (and $\lambda_x/y \approx 8$ for the wall-normal velocity). When extending the analysis to both homogeneous directions in x and y , the peak coherence is centred at $\lambda_x/\lambda_z \approx 2$ and $\lambda_x/\lambda_z \approx 1$ for p_w and u , and p_w and v , respectively. A stronger coherence is retrieved when the quadratic term of the wall pressure is concerned, but there is only little evidence for a wall-attached-eddy type of scaling. An experimental dataset comprising simultaneous measurements of wall pressure and velocity complements the DNS-based findings at one value of $Re_\tau \approx 2k$, with ample evidence that the DNS-inferred correlations can be replicated with experimental pressure data subject to significant levels of (acoustic) facility noise. It is furthermore shown that velocity-state estimations can be achieved with good accuracy by including both the linear and quadratic terms of the wall pressure. An accuracy of up to 72 % in the binary state of the streamwise velocity fluctuations in the logarithmic region is achieved; this corresponds to a correlation coefficient of ≈ 0.6 . This thus demonstrates that wall-pressure sensing for velocity-state estimation – e.g. for use in real-time control of wall-bounded turbulence – has merit in terms of its realization at a range of Reynolds numbers.

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Key words: boundary layer structure, turbulent boundary layers, turbulence control

1. Introduction

Inspiration for this work was born out of practical considerations associated with the implementation of real-time flow control for the reduction of skin-friction drag in wall-bounded turbulence. Efforts in turbulence control comprise both passive and active methods to target near-wall structures that scale in viscous units, $l^* \equiv \nu/u_\tau$, where $u_\tau \equiv \sqrt{\tau_w/\rho}$ is the friction velocity and ρ and ν are the fluid's density and kinematic viscosity, respectively. Leaving passive techniques aside, most studies on active skin-friction control tailor (statistical) forcing techniques to the inner scales (not requiring any sensing, e.g. Choi, DeBisschop & Clayton 1998; Kasagi, Suzuki & Fukagata 2009; Choi, Jukes & Whalley 2011; Bai *et al.* 2014); we refer to this as 'predetermined forcing control'. Only a few studies do incorporate sensing in numerical (Choi, Moin & Kim 1994; Lee, Kim & Choi 1998) and experimental (Rathnasingham & Breuer 2003; Qiao, Wu & Zhou 2018) 'real-time control' efforts of the near-wall structures. This approach requires that sensors and actuators are sized to said near-wall structures, which are roughly $500l^*$ in length and $100l^*$ in width. On practical engineering systems such as on an aircraft in cruise, $Re_\tau \approx 80k$ at a typical location for control on the fuselage (here $Re_\tau \equiv \delta u_\tau/\nu$, with δ being the boundary layer thickness). As such, control of the near-wall scales requires sensors/actuators with a spatial scale of ~ 0.1 mm (e.g. the size of sensors/actuators) and with a temporal scale in excess of 30 kHz (e.g. the frequency of actuation). This required spatial-temporal resolution of sensors and actuators is out of reach for current technologies. In addition, even if near-wall scales can be sensed and partially disrupted, the flow is expected to recover to the uncontrolled state within a streamwise distance that scales in viscous units (recall the auto-regeneration mechanisms of near-wall turbulence (Hamilton, Kim & Waleffe 1995), and see the study by Qiao *et al.* (2018) in which the controlled skin-friction drag recovers in less than 100 viscous units). Hence, the number of control stations for achieving streamwise-persistent control is also impractical. To overcome these issues, alternative control strategies emerged in tandem with studies of higher-Reynolds-number wall turbulence. A direct numerical simulation (DNS) study by Schoppa & Hussain (1998) utilized spanwise jets for predetermined, large-scale forcing control and reported drag reductions of up to 50 %. However, the low Reynolds number of $Re_\tau = 180$ yielded a negligible large-scale energy content in terms of the bulk turbulence kinetic energy (TKE), and recent investigations debate the effectiveness at higher Re_τ (Canton *et al.* 2016; Deng, Huang & Xu 2016; Yao, Chen & Hussain 2018). With higher-Reynolds-number studies available to date, experimental efforts to control flow structures within the logarithmic region in real time were undertaken (Abbassi *et al.* 2017). Even though the mean friction was favourably affected, the net energy savings of such control systems are difficult to assess and generalize.

Independent of the implementation or large-scale control, the theoretical work of Renard & Deck (2016) outlines the potential of this pathway in an elegant manner: their kinetic-energy budget analysis reveals how the skin-friction drag relates to different physical phenomena across the boundary layer. Due to the decay of the relative contributions of the buffer and wake regions to the TKE production with increasing Re_τ (Smits, McKeon & Marusic 2011a), the generation of the turbulence-induced excess friction is dominated by the dynamics in the logarithmic region. Hence, the work of

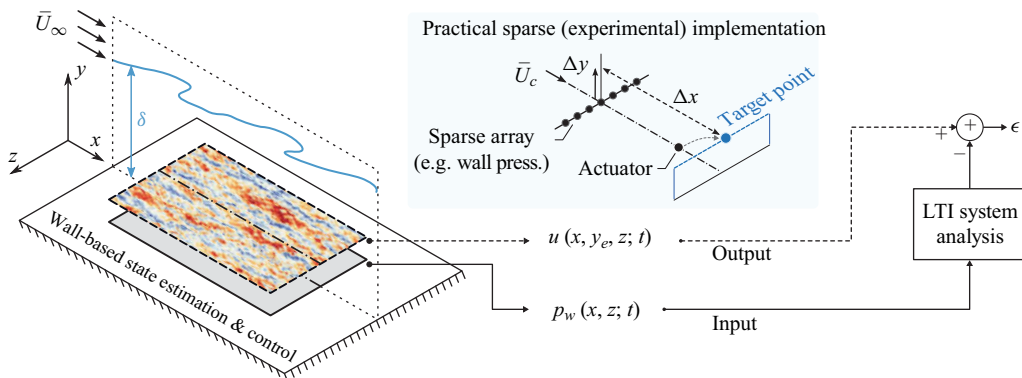


Figure 1. Wall-based quantities are to be used for a linear time-invariant (LTI) system analysis to estimate the state of the off-the-wall turbulent velocities. A sparse implementation considers a limited number of sensors/actuators, and includes typical offsets in the wall-normal (Δy) and streamwise (Δx) directions between the sensing location and the controller's 'target point.'

Renard & Deck (2016) suggests that drag reduction strategies targeting the TKE production mechanisms in that layer are worth investigating.

A controller's ability to selectively target certain turbulent structures depends on the degree of coupling between off-the-wall flow quantities within the linear, buffer and/or logarithmic regions of the flow, and observable wall quantities (sensors should be flush within the wall to avoid parasitic drag). When working towards realistic set-ups, a real-time control system with discrete sensors and actuators is the most logical (components should still be wall embedded to minimize parasitic drag, but the entire wall itself is not used for conducting the control action). In addition, when bringing in the requirement to (selectively) manipulate structures (e.g. Abbassi *et al.* 2017), a controller has to operate with an unavoidable wall-normal separation, Δy , between the sensing location and the 'target point' (figure 1). Likewise, a separation in the streamwise direction, Δx , must be adopted to account for control latency. These spatial separations result in a loss of correlation between the controller's input and the grazing turbulent velocities. Therefore, a sound understanding of (the scaling of) wall-pressure–velocity correlations is a prerequisite for designing a successful control system based on wall-pressure input data.

The notation in this paper is as follows. Coordinates x , y and z denote the streamwise, wall-normal and spanwise directions of the flow, and u , v , w and p represent the Reynolds decomposed fluctuations of the three velocity components and the static pressure, respectively. The wall pressure is denoted as p_w . Overlined capital symbols, e.g. \bar{U} , are used for the absolute mean. When quantities are presented in outer-scaling, length scale δ and velocity scale \bar{U}_∞ are used, while a viscous scaling is signified with superscript '+' and comprises a scaling with length scale $l^* = \nu/u_\tau$ and velocity scale u_τ .

1.1. Wall-pressure–velocity correlations

When attempting large-scale control of wall-bounded turbulence based on wall-pressure input data, a first step is to estimate a dynamic state of logarithmic-region turbulence from said fluctuating wall pressure, p_w . The velocity fluctuations themselves form the true state. Many studies are concerned with scaling laws and modelling attempts of pressure fluctuations (e.g. Willmarth 1975; Farabee & Casarella 1991; Klewicki, Priyadarshana

& Metzger 2008; Hwang, Bonness & Hambric 2009), but only very few works are concerned with an assessment of the instantaneous or statistical coupling between the velocity fluctuations and the wall pressure. Thomas & Bull (1983) revealed characteristic wall-pressure signatures associated with the near-wall burst-sweep events. Throughout the last decade, high-resolution mappings of the spatio-temporal pressure–velocity correlation have been reported (Ghaemi & Scarano 2013; Naka *et al.* 2015), but for a specific Re_τ condition. More recently, input–output linear time-invariant (LTI) system analyses have been conducted in the experimental works of Van Blitterswyk & Rocha (2017) and Gibeau & Ghaemi (2021). Nevertheless, no studies exist to date addressing the scaling of input–output relations, as a function of y and Re_τ . It is challenging to simultaneously acquire velocity and (noise-free) pressure data, particularly in wall-parallel planes as shown in figure 1, while such data are needed for examining wall-pressure–velocity correlations as a function of the streamwise and spanwise wavenumbers. Novel experiments can be designed to yield two-dimensional (2-D) coherence spectra (see Deshpande *et al.* 2020 for velocity–velocity correlations), but these are not trivial to perform. Given the current knowledge gap on wall-pressure–velocity coupling, our work covers an LTI-system analysis using high-fidelity data available from DNS campaigns.

A model transfer kernel between wall pressure and velocity is particularly useful for wall-based estimations of turbulent velocities. Upon confining the analysis to stochastic estimation-based techniques, these have proven to be useful for estimating large-scale features in turbulent flows using sparse input data. First-order techniques, known as linear stochastic estimation (LSE), were initially introduced in the turbulence community to inspect coherent turbulent structures in shear flows (Adrian 1979; Adrian & Moin 1988). Linear stochastic estimation can be implemented following a single- or multi-offset approach (Ewing & Citriniti 1999), in which the latter is identical to a spectral approach (see Tinney *et al.* 2006). The transfer kernel of the spectral LSE approach accounts for a gain and offset (or phase) per temporal and/or spatial scale, depending on the implementation. In view of figure 1, an LSE of an off-the-wall velocity field $u(x, y_e, z)$ at an estimation position y_e starts with a 2-D spatial Fourier transform of the unconditional input field $p_w(x, z)$,

$$P_w(\lambda_x, \lambda_z) = \mathcal{F}[p_w(x, z)]. \quad (1.1)$$

A spectral-domain estimate is then formulated as

$$\hat{U}_{LSE}(\lambda_x, \lambda_z, y_e) = H_L(\lambda_x, \lambda_z, y_e)P_w(\lambda_x, \lambda_z), \quad (1.2)$$

and the physical-domain estimate is found through the inverse Fourier transform,

$$\hat{u}_{LSE}(x, y_e, z) = \mathcal{F}^{-1}[\hat{U}_{LSE}(\lambda_x, \lambda_z, y_e)]. \quad (1.3)$$

The stochastic and complex-valued linear kernel in (1.2) is computed *a priori* and is equal to the wall-pressure–velocity cross-spectrum, ϕ_{up_w} , divided by the wall-pressure input spectrum, $\phi_{p_wp_w}$, following

$$H_L(\lambda_x, \lambda_z, y_e) = \frac{\phi_{up_w}(\lambda_x, \lambda_z, y_e)}{\phi_{p_wp_w}(\lambda_x, \lambda_z)}. \quad (1.4)$$

Throughout this paper a spectrum is defined as $\phi_{up_w}(\lambda_x, \lambda_z, y_e) = \langle U(\lambda_x, \lambda_z, y_e)P_w^*(\lambda_x, \lambda_z) \rangle$; capital quantities refer to the Fourier transform, $U = \mathcal{F}[u]$, the asterisk $*$ indicates the complex conjugate and $\langle \cdot \rangle$ denotes ensemble averaging.

To deduce how much energy of the LTI-system's output can be estimated, the linear coherence spectrum between the input and output data is insightful, and is defined as

$$\gamma_{up_w}^2(\lambda_x, \lambda_z, y_e) = \frac{|\phi_{up_w}(\lambda_x, \lambda_z, y_e)|^2}{\phi_{uu}(\lambda_x, \lambda_z, y_e)\phi_{p_wp_w}(\lambda_x, \lambda_z)} \in [0, 1]. \quad (1.5)$$

Using (1.4) the coherence can be rewritten as $\gamma_{up_w}^2 = |H_L|^2 \phi_{p_wp_w} / \phi_{uu}$. In a stochastic sense, the coherence magnitude is thus interpreted as the energy in the estimated output signal ($|H_L|^2 \phi_{p_wp_w}$), relative to the true output energy (ϕ_{uu}). An assessment of the coherence between the wall pressure and the turbulent velocities will address whether a substantial amount of energy in the turbulent fluctuations can be estimated.

So far, only the linear wall-pressure term was considered and this confines the analysis to scale-by-scale interactions. Linear stochastic estimation must be extended to a quadratic stochastic estimation (QSE) when nonlinearities manifest themselves in the input–output relation. Naguib, Wark & Juckenhöfel (2001) methodized a time-domain QSE and showed that the quadratic terms are critical for satisfactory estimates of the conditional streamwise velocity based on wall-pressure events in turbulent boundary layer (TBL) flows. Another example of improved estimates with QSE over LSE includes the estimate of velocities in a cavity shear layer, based on wall pressure (Murray & Ukeiley 2003, 2004; Lasagna, Orazi & Iuso 2013). By including the second-order, quadratic term in the stochastic estimate, a QSE procedure for the off-the-wall velocity field is formulated as

$$\hat{U}_{QSE}(\lambda_x, \lambda_z, y_e) = \underbrace{H'_L(\lambda_x, \lambda_z, y_e)P_w(\lambda_x, \lambda_z)}_{\text{linear term}} + \underbrace{H_Q(\lambda_x, \lambda_z, y_e)P_{w^2}(\lambda_x, \lambda_z)}_{\text{quadratic term}}. \quad (1.6)$$

When the skewness of the wall pressure is zero, it can be shown that the linear kernel in (1.6) is identical to (1.4), thus $H'_L = H_L$. For details, we refer to Naguib *et al.* (2001) and reported observations of negligible wall-pressure skewness (Gravante *et al.* 1998; Tsuji *et al.* 2007; Klewicki *et al.* 2008). Regarding the quadratic term, this one consists of the Fourier transform of the quadratic wall pressure, $P_{w^2}(\lambda_x, \lambda_z) = \mathcal{F}[p_w^2(x, z)]$. The pressure-squared term p_w^2 is computed as the square of the de-meaned wall-pressure field. The quadratic kernel $H_Q(\lambda_x, \lambda_z, y_e)$ is computed based on the same wall-pressure-squared term, following (1.7), and under the condition that the wall-pressure skewness is negligible.

$$H_Q(\lambda_x, \lambda_z, y_e) = \frac{\phi_{up_w^2}(\lambda_x, \lambda_z, y_e)}{\phi_{p_wp_w^2}(\lambda_x, \lambda_z)}. \quad (1.7)$$

Naguib *et al.* (2001) attributed the significant improvement of their conditional estimates of streamwise velocity fields based on wall-pressure events – with the inclusion of the quadratic pressure term – to the non-negligible turbulent–turbulent source (the ‘slow’ nonlinear pressure source associated with large-scale motions). This was analysed by considering the wall-pressure dependence on the turbulent flow field, following the solution of Poisson's equation for incompressible flow. When estimates were based on wall-shear stress, quadratic terms were less crucial (Adrian, Moin & Moser 1987; Guezennec 1989). Naguib *et al.* (2001) hypothesized that the portion in the estimate from the quadratic term represents a flow structure obeying outer scaling. However, they remained inconclusive due to their relatively small-Reynolds-number range.

1.2. Present contribution and outline

In summary, the extent of coupling between wall pressure and velocity at various friction Reynolds numbers in wall-bounded turbulence remains undetermined. Detailing the stochastic coupling, with linear and quadratic wall-pressure terms, is critical for gaining practical insight into whether a control system that relies on wall-pressure input has merit for real-time estimating (and controlling) large-scale structures in the logarithmic region. Albeit a wide variety of estimation techniques can be applied, such as physics-informed models (e.g. based on linearized Navier–Stokes equations (NSE) Madhusudanan, Illingworth & Marusic 2019), resolvent-based methods assimilating nonlinearity of the NSE (Arun, Bae & McKeon 2023) or neural networks (Guastoni *et al.* 2021), the simplicity of the LTI-system analysis allows for interpretability.

This work is structured as follows. First, DNS data are presented in § 2.1 and analysed through an input–output LTI-system approach in § 3 to infer Reynolds-number scaling relations for the wall-pressure–velocity correlations. Experimental wall pressure and velocity data are also described (§ 2.2) and assessed to identify whether the correlations can be replicated with experimental pressure data that are subject to significant levels of (acoustic) facility noise. Subsequently, the accuracy of velocity-state estimations is covered in § 4, and this aspect of wall-pressure sensing for estimation is of high practical relevance when addressing whether control based on wall pressure is a realistic route forward for real-time control.

2. Numerical and experimental data

2.1. Direct numerical simulations of turbulent channel flows

Four incompressible turbulent channel flow datasets are used and span one decade in Reynolds number, $Re_\tau \approx 550$ –5200. Details on the numerical scheme, resolution and turbulence statistics are documented by Lee & Moser (2015, 2019), and parameters of the DNS data and case names are summarized in table 1. In relevance to the current work involving pressure, the static pressure fields were obtained by solving the Poisson equation,

$$\frac{\partial^2 p}{\partial x_k \partial x_k} = -\rho \frac{\partial^2 u_i u_j}{\partial x_i \partial x_j}, \quad (2.1)$$

based on the full velocity field at each instant snapshot. Neumann boundary conditions were applied at the walls, following

$$\frac{\partial p}{\partial y} = \nu \frac{\partial^2 v}{\partial y^2}. \quad (2.2)$$

Finally, the average pressure in the homogeneous directions was set according to

$$\langle p \rangle = -\rho \langle v^2 \rangle + C. \quad (2.3)$$

Here, $\langle \cdot \rangle$ denotes the average in the homogeneous direction and the integration constant C is set to zero for convenience. Later on, not only wall-pressure fields are used but also fields of the wall-pressure squared p_w^2 . Such nonlinear products during simulations and post-processing steps were generated using a 3/2 de-aliasing rule with zero padding (Orszag 1971). Details of the pressure field computations are described in Panton, Lee & Moser (2017).

For reference, one-dimensional (1-D) spectrograms of u , v and p are presented in figure 2(a–c), with isocontours of the premultiplied spectrum, e.g. $k_x^+ \phi_{uu}^+$. Four sets of

Numerical data: Channel DNS of Lee & Moser (2015)					
Case:	R0550	R1000	R2000	R5200	
Re_τ	544	1000	1995	5186	
$(L_x, L_z)/\delta$	$(8\pi, 3\pi)$	$(8\pi, 3\pi)$	$(8\pi, 3\pi)$	$(8\pi, 3\pi)$	
Δx^+	8.9	10.9	12.2	12.7	
Δz^+	5.0	4.6	6.1	6.4	
$\Delta y_w^+, \Delta y_c^+$	0.019, 4.5	0.019, 6.2	0.017, 8.2	0.498, 10.3	
Tu_τ/δ^\dagger	13.6	12.5	11.5	7.80	
Experimental data: TBL at $x = 3.07$ m in the W tunnel					
Boundary layer	Hot wire			Microphones	
Re_τ	2280	Type	Dantec 55P15	Type	GRAS 46BE
Re_θ	6190	l^+	42.4	d^+	13.6
\bar{U}_∞	14.8 m s^{-1}	l/d	250	f_r^+	0.15
δ	67.3 mm	ΔT^+	0.36	ΔT^+	0.36
u_τ	0.54 m s^{-1}	$T\bar{U}_\infty/\delta$	32 860	$T\bar{U}_\infty/\delta$	32 860
$l^* = \nu/u_\tau$	29.5 μm	—	—	—	—

Table 1. Parameters of data sets used: channel DNS data and experimental TBL data. Note that δ for DNS of the channel flows and the boundary layer experiment denote the channel half-width and the boundary layer thickness, respectively. † Total simulation time without transition.

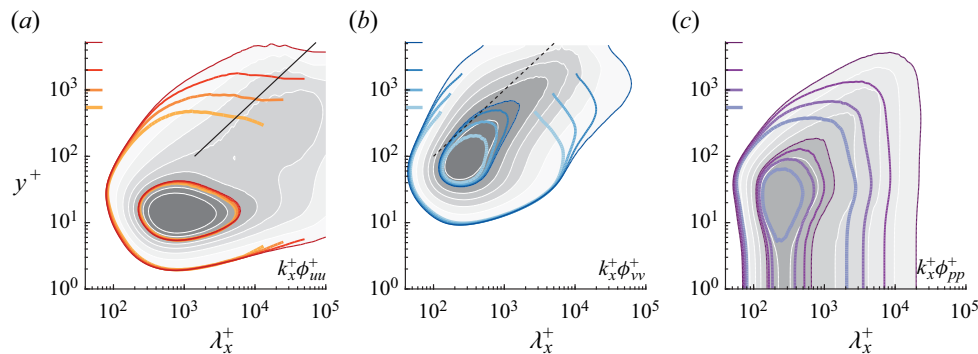


Figure 2. One-dimensional spectrograms of (a) u , (b) v and (c) p . Two clusters of solid, coloured isocontours on (a–c) correspond to two contour values of $k_x^+ \phi_{uu}^+ = [0.2; 1.2]$, $k_x^+ \phi_{vv}^+ = [0.05; 0.3]$ and $k_x^+ \phi_{pp}^+ = [0.45; 2.25]$, respectively, for all Re_τ cases (an increased colour intensity corresponds to an increase in Re_τ ; the channel half-widths $\delta^+ = Re_\tau$ are indicated along the ordinate). The grey-scale contour shows a finer discretization of isocontours for the R5200 case only.

coloured isocontours at the two values indicated in the caption correspond to the four Reynolds-number cases, and the small lines at the ordinates correspond to each $Re_\tau \equiv \delta^+$. Only for the highest-Reynolds-number case, R5200, a finer discretization of grey-filled contours is shown. Data are presented in a similar manner later on in § 3.

As is well known, the most energetic content resides at $y^+ \approx 15$ and $\lambda_x^+ \approx 10^3$ for the streamwise velocity, and $\lambda_x^+ \approx 250$ for the wall-normal velocity and wall pressure. The pressure spectrum remains constant for $y^+ \lesssim 5$, reflecting the wall-pressure spectrum. For all fluctuating quantities in figure 2, their variance, at a given y^+ , grows due to additional energy at large λ_x^+ . For instance, see Mathis, Hutchins & Marusic (2009) for the scaling

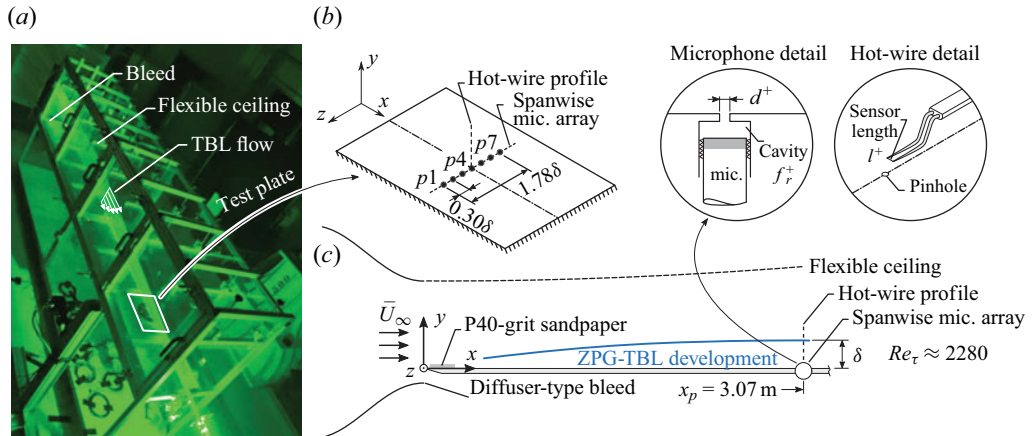


Figure 3. (a) Set-up for the ZPG-TBL studies in the W tunnel. (b,c) Experimental arrangement with a single hot-wire probe and a pinhole-mounted microphone array measuring the wall pressure at seven spanwise positions. In addition, one microphone is placed in the free stream to measure the facility (acoustic) noise.

of u spectrograms and Panton *et al.* (2017) for the scaling of the mean-square pressure fluctuations.

2.2. Experimental wall-pressure–velocity data

Experiments were carried out in the W-tunnel facility within the Faculty of Aerospace Engineering at the Delft University of Technology. This open-return tunnel has a contraction ratio of 4.7 : 1, with a square cross-sectional area of $0.60 \times 0.60 \text{ m}^2$ at the inlet of the test section, and can produce a maximum flow velocity of roughly 16.5 m s^{-1} . For generating a TBL flow, a set-up was developed with a relatively long streamwise development length, consisting of a metal frame with polycarbonate walls for optical access (figure 3a). The bottom wall has a width of 0.60 m and a total length of 3.75 m. The TBL was initiated just downstream of the leading edge at $x = 0$ with a trip of P40-grit sandpaper over a length of 0.115 m and over the full perimeter. The floor was suspended 0.08 m above the bottom wall of the upstream tunnel contraction, allowing for a clean start of the TBL flow without leading-edge separation. A flexible, 4 mm thick polycarbonate ceiling was configured for a zero-pressure gradient (ZPG) development of the TBL. This ZPG condition was assessed using the acceleration parameter $K = (\nu/U_e^2)(d\bar{U}_e/dx)$, where $\bar{U}_e(x)$ is the boundary layer edge velocity. A Pitot-static tube in the potential flow at $x_p = 3.07 \text{ m}$ provided measures of the total (p_0) and static (p) pressures, and thus, $\bar{U}_\infty = \bar{U}_e$ at x_p (the static temperature and barometric pressure were also recorded for inferring the air density and viscosity). Using two streamwise rows of (in total) 100 static pressure taps in the floor, providing $p(x)$, the variation in $\bar{U}_e(x)$ was computed as $\bar{U}_e(x) = \sqrt{2(p_0 - p(x))/\rho}$, given that the total pressure remains constant along a streamline. For the nominal free-stream velocity of the current study ($\bar{U}_\infty \approx 15 \text{ m s}^{-1}$), the acceleration parameter remained within an acceptable range for a ZPG condition along the entire test section ($K < 1.6 \times 10^{-7}$ following Schultz & Flack 2007). Finally, measurements are performed near the aft of the set-up around $x_p = 3.07 \text{ m}$. Here, the free-stream turbulence intensity at the nominal free-stream velocity, based on the hot-wire measurement described later, is $\sqrt{u^2}/\bar{U}_\infty \approx 0.3 \%$.

Hot-wire anemometry measurements were performed with a Dantec Dynamics 55P15 miniature-wire boundary layer probe. This single-wire probe only yields the streamwise velocity (given that $u \gg v$ in boundary layer flows) and comprised a plated Tungsten wire with a diameter of $d_w = 5 \mu\text{m}$ and a sensing length of $l = 1.25 \text{ mm}$ (resulting in $l/d_w = 250$). The viscous-scaled wire length of $l^+ = 42.4$ yields an acceptable spatial resolution (Hutchins *et al.* 2009), given that this study concentrates primarily on the logarithmic region for wall-pressure–velocity correlations (the measurement is fully resolved in that region, as shown later on). Hot-wire traversing was done with a Zaber X-LRQ300HL-DE51 traverse, with an integrated encoder and controller yielding a positional accuracy of $13 \mu\text{m}$ (a resolution better than $0.4l^*$). A Taylor-Hobson micro alignment telescope was used to position the hot wire at the most near-wall position before performing a wall-normal traverse spanning 40 logarithmically spaced positions in the range $10.2 \lesssim y^+ \lesssim 1.2Re_\tau$.

The hot wire was operated in constant temperature mode using a TSI IFA-300 bridge at an overheat ratio of 1.8. For each hot-wire position, signals were sampled (simultaneously with the wall-pressure sensors) at a rate of $\Delta T^+ \equiv u_\tau^2/\nu/f_s = 0.36$, where $f_s = 51.2 \text{ kHz}$ is the sampling frequency. The anemometer system low-pass filtered the voltage signal with a spectral cutoff at 20 kHz . Sampling was done with a 24-bit A/D conversion through an NI9234 module embedded in an NIcDAQ. Relatively long signals were acquired with an uninterrupted acquisition time of $T_a = 150 \text{ s}$ at each wall-normal position, resulting in more than $32\,860$ boundary layer turnover times; this is more than sufficient for converged spectral statistics at the lowest frequencies of interest. An *in-situ* calibration of the hot wire was performed in the potential flow region using the reference velocity provided by the Pitot-static tube. A correction method for hot-wire voltage drift due to variations in barometric pressure and static temperature was also implemented (Hultmark & Smits 2010).

Profiles of \bar{U} and \bar{u}^2 are plotted in figure 4(a) and the boundary layer parameters are listed in table 1. These parameters were obtained by fitting the mean velocity profile to a composite profile with log-law constants of $\kappa = 0.384$ and $B = 4.17$ (Chauhan, Monkewitz & Nagib 2009). On the basis of these values, $Re_\tau = 2280$ and the Reynolds-number based on the momentum thickness is $Re_\theta \equiv \bar{U}_\infty\theta/\nu = 6190$. A local friction coefficient of $C_f = 2u_\tau^2/\bar{U}_\infty^2 \approx 2.69 \times 10^{-3}$ matches a Coles–Fernholz relation, $C_f = 2[\frac{1}{0.38} \ln(Re_\theta) + 3.7]^{-2}$, to within 4.5 %. The mean velocity profile compares well to the R2000 case of the DNS, up to the wake region. From the streamwise turbulence intensity profile, it is clear that the experimental data are attenuated due to the hot wire’s spatial resolution. When correcting for this limited resolution via the method of Smits *et al.* (2011b), it matches well with the DNS profile in the buffer region and above, but a slight overestimate of the expected peak value at $y^+ \approx 15$ is observed, following $\bar{u}_{max}^2 = 0.63 \ln(Re_\tau) + 3.80$ (Lee & Moser 2015; Smits *et al.* 2021). We ascribe this mismatch to wall-proximity effects (Hutchins *et al.* 2009).

Prior to computing frequency spectra $\phi_{uu}(f)$, the experimental time series $u(y, t)$ were down-sampled with a factor of 5 to match the corrected wall-pressure data (see Appendix A). One-sided spectra $\phi_{uu}(y; f) = 2\langle U(y; f)U^*(y; f) \rangle$ were computed by way of ensemble averaging a total of 180 fast Fourier transform (FFT) partitions of $N = 2^{14}$ samples (50 % overlap and a Hanning window applied to them). This yields a spectral resolution of $df = 0.625 \text{ Hz}$ or $df^+ = 3.4 \times 10^{-5}$. For interpretive purposes, frequency spectra are converted to wavenumber spectra using a single convection velocity \bar{U}_c (taken as the local mean velocity $\bar{U}(y)$ unless stated otherwise). With wavenumber

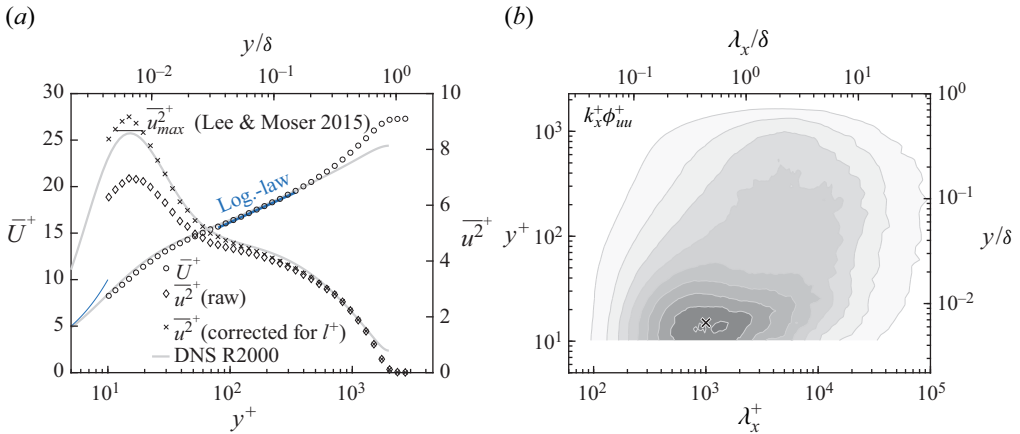


Figure 4. (a) Experimental boundary layer profiles of the streamwise mean velocity and turbulence intensity, compared with the DNS R2000 case. The mean velocity profile is compared with the log law with constants $\kappa = 0.384$ and $B = 4.17$, and the u -TKE profile is corrected for spatial resolution effects. (b) Premultiplied energy spectrogram $k_x^+ \phi_{uu}^+$ (filled isocontours 0.2:0.2:1.8); the scale axis is converted to a wavelength dependence using $\lambda_x = \bar{U}(y)/f$.

$k_x = 2\pi f/\bar{U}_c$ the wavenumber spectrum becomes $\phi_{uu}(k_x) = \phi_{uu}(f) df/dk$, where group $df/dk = \bar{U}_c/(2\pi)$ converts the energy density from a ‘per unit frequency’ to a ‘per unit wavenumber’ (the spectral resolution becomes $dk \approx 0.88 \text{ m}^{-1}$ or $dk^+ \approx 2.6 \times 10^{-5}$ at the lowest position of $y^+ = 10$). Throughout this paper, the scale axis is either presented in terms of k_x or wavelength $\lambda_x = 2\pi/k_x$. Figure 4(b) presents the streamwise energy spectrogram $k_x \phi_{uu}$ for validation of the experimental set-up. The inner-spectral peak is clearly visible and is identified with the \times marker at $\lambda_x^+ = 10^3$ and $y^+ = 15$. Larger scales are more energetic in the logarithmic region, although the Reynolds number is not yet high enough for a discernible outer-spectral peak to appear (Baars & Marusic 2020).

Wall-pressure measurements were simultaneously made with the hot-wire ones, and thus sampled with the parameters listed in table 1. Eight GRAS 46BE $\frac{1}{4}$ in. CCP free-field microphones were employed. Seven of them formed a spanwise array for wall-pressure measurements, while one was used in the potential flow region to measure facility noise. The microphone sets have a nominal sensitivity of 3.6 mV Pa^{-1} and a frequency response range with an accuracy of $\pm 2 \text{ dB}$ for 4 to 80 kHz, while for the range 10 Hz to 40 kHz, the accuracy is $\pm 1 \text{ dB}$. The dynamic range is 35 to 160 dB (with a reference pressure of $p_{ref} = 20 \text{ } \mu\text{Pa}$). For our current wall-pressure–velocity correlation study, the primary frequencies of interest lay between roughly 5 and 800 Hz, and the measured pressure intensity is of the order of 105 dB, thus making these microphones suitable for these types of measurements.

The spanwise array of seven equally spaced pinhole-mounted microphones had an inter-spacing of 20 mm, or 0.30δ , with the total width spanning $\Delta z = 1.78\delta$. The hot-wire profile was measured above the centre pinhole. Each microphone was screwed inside a cavity (after removal of the microphone grid cap) so that the sensing diaphragm formed the bottom of the cavity. On the back side, underneath the wind tunnel floor, a box surrounding the microphones prevented any pressure fluctuations at their venting holes. On the TBL side, a pinhole with a diameter of $d^+ = 13.6$ ($d = 0.40 \text{ mm}$) ensured a sufficient spatial resolution of the measurement (Gravante *et al.* 1998). The pinhole depth was $t = 0.80 \text{ mm}$ and the cavity diameter matched the microphone-body outer diameter ($D = 6.35 \text{ mm}$). The cavity length was designed as $L = 2.0 \text{ mm}$, so that the Helmholtz resonance frequency

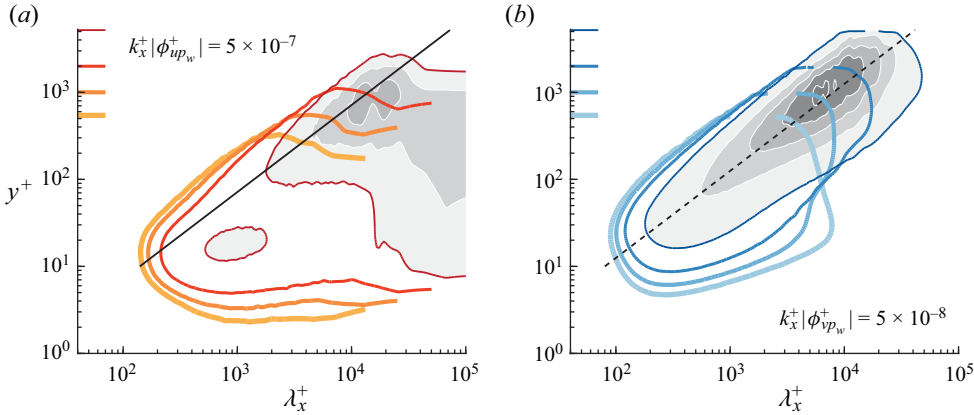


Figure 5. (a) One-dimensional gain of the cross-spectrogram, computed using u and p_w . Solid, coloured iso-contours correspond to one contour value indicated in the figure for all Re_τ cases (an increased colour intensity corresponds to an increase in Re_τ); the greyscale contour shows a finer discretization of iso-contours for the R5200 case only. A black trend line indicates a wall-scaling of $\lambda_x/y = 14$. (b) Similar to sub-figure (a), but now for v and p_w . A black-dashed trend line indicates a wall-scaling of $\lambda_x/y = 8$.

of the cavity was above the frequency range of interest ($f_r^+ = f_r v/u_\tau^2 = 0.15$ or $f_r = 2750$ Hz). Raw signals of the pinhole-microphone measurements required post processing to yield valid time series of the wall-pressure fluctuations. The post-processing steps are described in [Appendix A](#).

3. Scaling of the wall-pressure–velocity coupling

This section utilizes the DNS data to assess the coupling between the fluctuations of u and v , and the wall-pressure field p_w . First, we proceed with a 1-D spectral analysis in the streamwise direction, which is reminiscent of the data available from typical experiments.

3.1. One-dimensional analysis in the streamwise direction

Cross-spectra of wall pressure and velocity yields an indication of the coupling of absolute energy. We only examine the gain of the complex-valued 1-D cross-spectrum, $\phi_{up_w}(\lambda_x, y)$; the phase is beyond the scope of our current work and is only relevant for spatial/temporal lags. The gain of the cross-spectrogram is presented with isocontours of $|\phi_{up_w}^+|$ in [figure 5\(a\)](#). One particular contour value is chosen and the isocontours correspond to the four Reynolds-number cases of the DNS ([table 1](#)). It is evident that the region of cross-spectral energy grows along the black solid line with an increase in Re_τ . Since the black line indicates a constant ratio of λ_x/y , this trend is representative of distance-from-the-wall scaling.

A normalized coherence is now considered to explore how the coupling scales, independent of the scaling of u energy. The coherence

$$\gamma_{up_w}^2(\lambda_x, y) = \frac{|\phi_{up_w}(\lambda_x, y)|^2}{\phi_{uu}(\lambda_x, y)\phi_{p_wp_w}(\lambda_x)} \quad (3.1)$$

is presented in [figure 6\(a\)](#) using one isocontour of $\gamma_{up_w}^2$ for all four Re_τ of the DNS. For the highest-Reynolds-number case, R5200, grey-filled contours show that a spectral band of

strong coherence appears at a self-similar scaling of $\lambda_x/y \approx 14$; this scaling also appears to be Reynolds-number invariant. To further accentuate these observations, individual coherence spectra are superimposed in [figure 6\(c\)](#). Here, each bundle of lines with the same colour corresponds to one Reynolds-number dataset. Coherence spectra are plotted corresponding to a relatively coarse grid of y positions that are logarithmically spaced between lower and upper bounds of an extended logarithmic region, chosen as $y^+ = 80$ and $y^+ = 0.16Re_\tau$, respectively (resulting in 1 curve for the R0550 data and 15 curves for the R5200 data). A wall scaling of λ_x/y is adopted on the abscissa. It is evident that the coherence spectra collapse; signifying a Reynolds-number invariant location of the coherence peak and a constant coherence magnitude. This coherence-peak location at $\lambda_x/y = 14$ closely matches the Reynolds-number invariant aspect ratio of wall-attached coherent structures of u ; see Baars, Hutchins & Marusic (2017). The relatively low magnitude indicates a weak linear coherence, but this is expected given that (extreme) events in the wall pressure are primarily caused by sweeps, ejections, and thus, motions associated with strong vertical velocity fluctuations (and less so with u fluctuations). This can, for instance, be observed in the work by Ghaemi & Scarano (2013) where high-amplitude near-wall-pressure events are considered by visualizing the associated conditional pressure and velocity structures. In this regard, it is evident from [figure 7\(a\)](#) that the ‘self-similar scaling’ of coherence appears at its smallest scale near the wall with a peak at $y^+ \approx 15$ and $\lambda_x^+ \approx 14 \times 15 \approx 210$ (visualized with a round marker). This streamwise scale agrees with the typical (conditional) near-wall turbulent structure associated with these high-amplitude pressure peaks observed by Ghaemi & Scarano (2013).

By further inspection, it is intriguing to note the appearance of a region of zero coherence at relatively large wavelengths and at positions below the ridge, even though this region resides closer to the wall. It can thus be concluded that large-scale u fluctuations in close proximity to the wall do not comprise a phase-consistent linear relationship with the wall pressure, whereas the u fluctuations further up in the wall-bounded turbulent flow do. Presumably, this is due to the stronger dispersive (and random) nature of the convection of large-scale structures near the wall (Liu & Gayme 2020). The wall-pressure footprint for each scale is thus only linearly coupled to u fluctuations that are statistically self-similar and that govern the footprint from each respective height. This is consistent with the fact that the pressure scalar is influenced by the velocity field in the entire domain; this is opposite to, for instance, wall-attached velocity fluctuations that are coherent throughout the full wall-normal extent (Baars *et al.* 2017).

Finally, two dominant regions of non-zero coherence appear: (1) very near the wall at wavelengths $\lambda_x^+ \lesssim 200$ and at $y^+ \lesssim 5$, and (2) at large outer-scaled wavelengths (e.g. for $Re_\tau \approx 5200$ for wavelengths $\lambda_x^+ \gtrsim 3 \times 10^4$). Although these regions have a non-zero coherence, it is important to note that u has no significant energy in region 1 ([figure 2a](#)) and neither has p_w in region 2 ([figure 2c](#)). Likewise, the cross-spectral energy is low in these regions (recall [figure 5a](#)). Although insignificant in terms of absolute energy, very large global modes of velocity fluctuations spanning the entire wall-normal extent (and simulation box) can be responsible for the large-scale coherence in region 2 (del Álamo & Jiménez 2003; Jiménez & Hoyas 2008).

A correlation analysis for p_w with v (instead of u) results in the spectrograms of $|\phi_{vp_w}|$ and $\gamma_{vp_w}^2$ shown in [figures 5\(b\)](#) and [6\(b\)](#), respectively. As for p_w and u , coherence spectra for p_w with u are superimposed in [figure 6\(d\)](#), as a function of λ_x/y and for a range of y positions for all Reynolds-number datasets, to bring attention to the self-similar and Reynolds-number-invariant coherence peak near $\lambda_x/y = 8$. As for the u fluctuations,

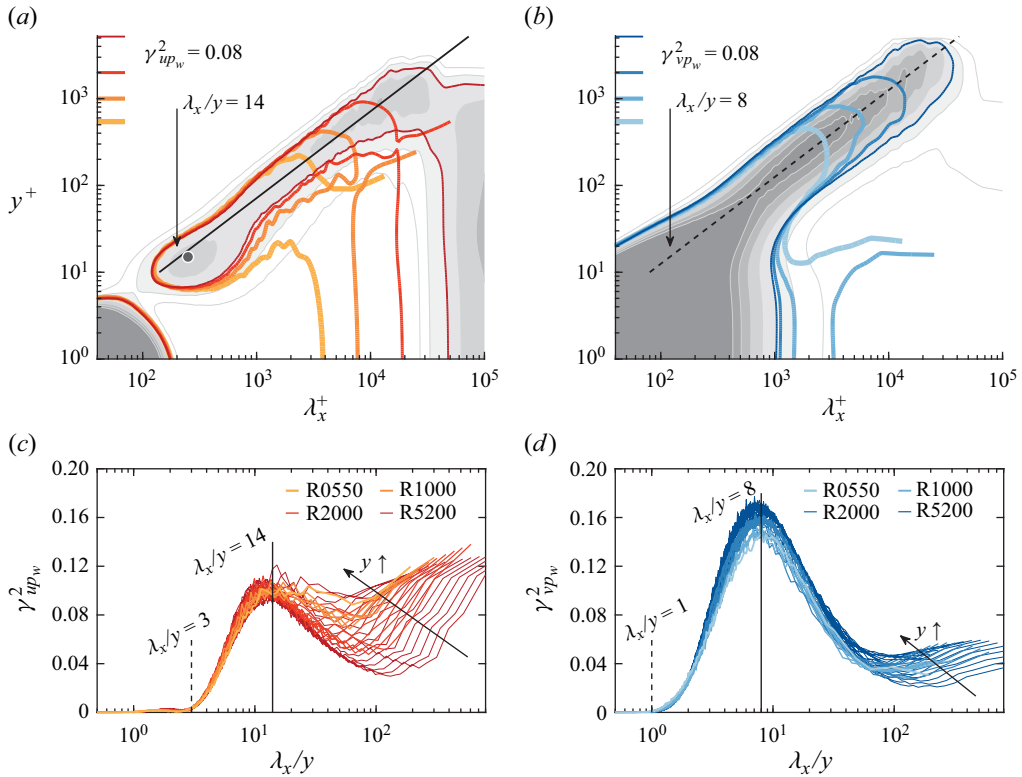


Figure 6. (a) Linear coherence of u and p_w . Solid, coloured isocontours correspond to one contour value for all Re_τ cases (an increased colour intensity corresponds to an increase in Re_τ); the grey-scale contour shows a finer discretization of contours for $Re_\tau \approx 5200$ only. (b) Similar to subfigure (a) but now for the linear coherence of v and p_w . (c) Linear coherence spectra $\gamma^2_{up_w}$ (one bundle of lines per Re_τ condition) within the logarithmic region, in the range $80 \lesssim y^+ \lesssim 0.15Re_\tau$. Results in frequency space are converted to a wavelength dependence using $\lambda_x \equiv \bar{U}(y)/f$. (d) Similar to subfigure (c) but now with the linear coherence spectra $\gamma^2_{vp_w}$.

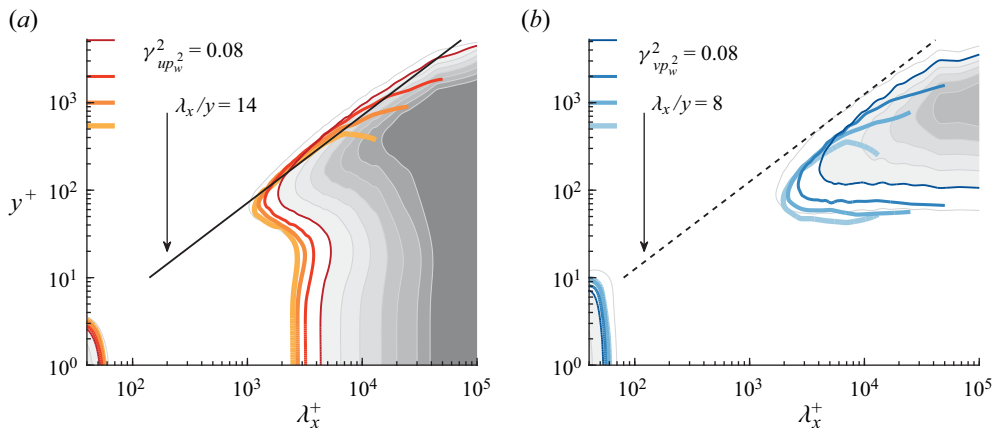


Figure 7. Similar to figure 6 but now for (a) u and p_w^2 (wall-pressure squared) and (b) v and p_w^2 .

a significant bulk of the coherence resides at small wavelengths very near the wall when p_w and v are concerned, but this coherence is insignificant given the absence of cross-spectral energy (figure 5b). The main finding that the wall-pressure-coherent energy in v resides at smaller wavelengths than their streamwise counterpart is interpreted as follows. Fluctuations in v induce wall-pressure fluctuations through a ‘flow stagnation’ when directed towards the wall. When wall-pressure-coherent velocity fluctuations are thought of as wall-attached motions (e.g. hairpins or packets of them), their centre regions contain $u < 0$, while the v fluctuations induced by the vortical motions of vortex heads inducing wall pressure reside at shorter λ_x (statistically thus nearly half the size). This is evident from spectra: while the peak in the uv cospectra resides around $\lambda_x/y \approx 15$ (dominated by the higher energy in u , residing at relatively large streamwise scales), the dominant energy in the spectra of v alone appears at much shorter scales throughout the logarithmic region, along $\lambda_x/y \approx 2$ (Baidya *et al.* 2017). In addition, Jiménez & Hoyas (2008) showed that pressure spectra scale relatively well with the local Reynolds shear stress \overline{uv}^2 (representative of the intensity of eddying motions). Given the relatively large streamwise scales in \overline{uv} and the fact that the wall-pressure spectrum embodies a footprint of the global pressure fluctuations, the peak coherence of p_w with v does indeed reside at slightly larger scales $\lambda_x/y \approx 8$ (than the peak location of the v spectra at $\lambda_x/y \approx 2$, see Baidya *et al.* 2017).

Higher-order terms of the wall-pressure–velocity coupling are of relevance to the analysis in § 4, when p_w forms the input for estimates of the velocity fluctuations. For this reason, coherence spectra of the wall-pressure squared, with both the u and v velocities, are presented as spectrograms in figures 7(a) and 7(b), respectively. It is important to note here that p_w^2 is the square of the de-meaned wall pressure (this is not the same as the de-meaned wall-pressure squared). Note that this form of a nonlinear correlation does address interactions of different scales (e.g. an interscale interaction of pressure with velocity), although not explicitly in terms of triadic (or higher-order) scale interactions. Bipectral analysis is required to address those interactions (Baars & Tinney 2014; Cui & Jacobi 2021), which is beyond the scope of this paper. Focusing on the coherence of p_w^2 with u , Naguib *et al.* (2001) had hypothesized that this quadratic pressure interaction represents a flow structure obeying outer scaling. Trends of $\gamma_{up_w^2}^2$ show a self-similar scaling in the logarithmic region ($y^+ \gtrsim 100$) and coherence only appears for $\lambda_x \gtrsim 14y$; note that this corresponds to the region where $\gamma_{up_w}^2$ starts to decrease from its peak ridge at $\lambda_x/y = 14$. A distance-from-the-wall scaling is also seen in the trends of $\gamma_{vp_w^2}^2$, which appears to become relevant at scales slightly larger than $\lambda_x/y = 8$ (the lowest locations at which $p_w v$ coherence appears is not fixed in outer scaling).

Physically, the coherence at relatively large scales involving p_w^2 would be reminiscent of nonlinearities associated with an intensity-modulation phenomenon (Tsuji *et al.* 2007). This modulation of the near-wall quantities in wall-bounded turbulence is induced by large-scale velocity fluctuations that are most energetic in the logarithmic region (and are most pronounced at high values of Re_τ) and that leave a direct imprint on the wall. This imprint changes the local, large-scale friction velocity and, thus, the viscous scale. Consecutively, this yields modulated near-wall pressure and small-scale velocity fluctuations given that these near-wall quantities are universal in viscous scaling (Zhang & Chernyshenko 2016; Chernyshenko 2021). Thus, when the intensity of (wall-)pressure fluctuations are modulated by the large-scale u (or v) fluctuations, the intensity-modulation ‘envelope’ (which by itself has no energy contribution in p_w) becomes energetic in the square of the de-meaned wall-pressure signal, p_w^2 . At the same time, the usage of p_w^2 results

in linear coherence at wavelengths larger than where the coherence peaks with the linear pressure term (figure 7*a,b*). Further inspection of figure 7 reveals that the coherence is strongest for the velocity fluctuations taken in the logarithmic region; this reflects the general consensus in the community that the modulation of wall quantities is driven by energetic large-scale motions in the logarithmic region of the flow. As a final note, we confirmed that the coherence with any higher-order pressure terms (p_w^3 with either u or v) was zero.

3.2. Two-dimensional analysis in the streamwise–spanwise plane

In the 1-D spectral analysis, all spanwise information was lumped together. To inspect the full spectral picture in both homogeneous directions, we move towards a 2-D analysis. At first the 2-D spectrograms of the streamwise velocity, $\phi_{uu}(\lambda_x, \lambda_z, y)$, and wall pressure, $\phi_{p_w p_w}(\lambda_x, \lambda_z)$, are shown for $y^+ \approx 80$ at $Re_\tau \approx 5200$ in figures 8(*a*) and 8(*b*), respectively. A solid black line in figure 8(*a*) indicates a scaling of $\lambda_x/\lambda_z = 2$ whereas the dashed line in figure 8(*b*) signifies a scaling of $\lambda_x/\lambda_z = 1$. Energy in u at larger wavelengths is more anisotropic at this position in the near-wall region and constitutes larger streamwise scales than spanwise scales. This is reminiscent of (very) large-scale motions in the streamwise direction. The wall pressure reflects a more isotropic behaviour in the two homogeneous directions, owing to the fact that wall pressure has a stronger coupling with the v motions, which are themselves more isotropic than u motions. Nevertheless, the scope of the current paper is to inspect the normalized coherence, since this reveals the degree of phase consistency and, thus, the energy fraction of the velocity fluctuations that are stochastically coupled to the wall pressure. Coherence in two dimensions is a generalization of (3.1), following

$$\gamma_{up_w}^2(\lambda_x, \lambda_z, y) = \frac{|\phi_{up_w}(\lambda_x, \lambda_z, y)|^2}{\phi_{uu}(\lambda_x, \lambda_z, y)\phi_{p_w p_w}(\lambda_x, \lambda_z)} \in [0, 1]. \quad (3.2)$$

Coherence for the data used to present the 2-D (auto-)spectrograms in figure 8(*a,b*) is shown in figure 8(*d*). Notably, the coherence only appears for $\lambda_x^+ \gtrsim 400$ (when taking a threshold of $\gamma_{up_w}^2 = 0.05$), agreeing to what was observed from the 1-D analysis in figure 6. A coherence peak in the 2-D view still resides close to $\lambda_x/y \approx 14$ (for figure 8*d* equivalent to $\lambda_x^+ = 14y^+ = 1120$) and is reasonably symmetric around $\lambda_x/\lambda_z = 2$. The latter implies that wall-pressure-coherent u motions are roughly twice as long as they are wide. Another region of peak coherence resides at very large λ_z , but the energy there is insignificant and, hence, this high coherence is physically irrelevant. For instance, at $(\lambda_x^+, \lambda_z^+) = (10^3, 10^4)$ in figure 8(*d*), $\gamma_{up_w}^2 \approx 0.25$ even though the absolute energy of u is invisible in figure 8(*a*). For the v motions (auto-spectrogram shown in figure 8*c*) the 2-D coherence in figure 8(*e*) shows symmetry around $\lambda_x/\lambda_z = 1$. A further statistical interpretation is reserved for when the 2-D coherence is presented in a different manner, described next.

So far, 2-D auto-spectrograms were premultiplied with $k_x k_z$ and visualized with isocontours of $k_x k_z \phi$ in a log-Cartesian space. This visualization ensures that the ‘area under the contour’ is proportional to the energy residing in logarithmic ranges of λ_x and λ_z . Lee & Moser (2019) pointed out that this method of visualization also comes with two primary shortcomings. In summary, the distortion of the 2-D wavevector orientation complicates observing the alignment of modes with the x and z directions: all lines of constant λ_x/λ_z (or k_z/k_x) have a slope of 1 and are only marginally offset on the log–log plot, for different constants of λ_x/λ_z (see figure 8*b*). In addition, vector wavelengths

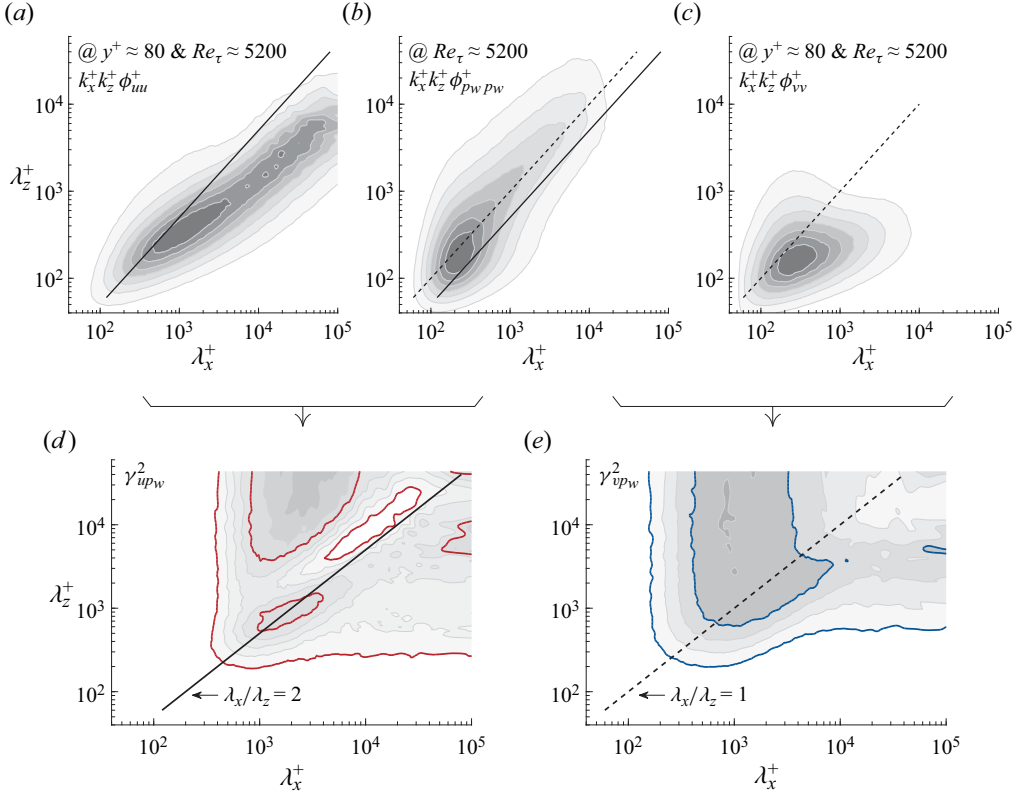


Figure 8. Two-dimensional spectrograms of (a) u , (b) p_w and (c) v at one Re_τ and y^+ , as indicated in the subfigures; grey-filled contours show seven isocontours ranging up to the maximum value. (d) Two-dimensional linear coherence of u and p_w , for the same Re_τ and y^+ as (a,b); the solid, coloured isocontours correspond to two contour values of $\gamma^2_{upw} = [0.05; 0.25]$. (e) Similar to subfigure (d) but now for the 2-D linear coherence of v and p_w ; the solid, coloured isocontours correspond to two contour values of $\gamma^2_{vpw} = [0.10; 0.30]$.

with a similar magnitude $\lambda = (\lambda_x^2 + \lambda_z^2)^{1/2}$ follow a non-trivial trend line that creates difficulties in assessing scale isotropy. That is, when turbulence quantities contain an equal energy content at vector wavelengths (or wavenumbers) that have the same magnitude in the wall-parallel plane, this energy is said to be distributed isotropically in scale. Because of the two shortcomings, Lee & Moser (2019) introduced a ‘log-polar’ format for the 2-D spectrum. When considering wavenumbers, $\phi(k_x, k_z)$ can be expressed in polar coordinates, yielding $\phi(k \cos \theta, k \sin \theta)$ with $k_x = k \cos(\theta)$ and $k_z = k \sin(\theta)$. When defining $\xi = \log_{10}(k/k_{ref})$, where k_{ref} is a reference wavenumber smaller than the smallest non-zero wavenumber considered, a set of logarithmic polar coordinates would be ξ and θ , with associated Cartesian coordinates $k_x^\# = \xi \cos \theta = \xi k_x/k$ and $k_z^\# = \xi \sin \theta = \xi k_z/k$, respectively. Following Parseval’s theorem, the spectral integral equals

$$\int_{k_x > 0} \int_{k_z > 0} \phi \, dk_x \, dk_z = \int_{\theta=0}^{\pi/2} \int_{\xi > 0} \frac{k^2}{\xi} \phi \, d\xi \, d\theta = \int_{k_x^\# > 0} \int_{k_z^\# > 0} \frac{k^2}{\xi} \phi \, dk_x^\# \, dk_z^\#. \quad (3.3)$$

Hence, to preserve the total energy in plotting, quantity $k^2 \phi / \xi$ is visualized with linear axes $k_x^\#$ and $k_z^\#$. Hence, lines of constant k_z/k_x possess slopes of k_z/k_x , and a curve of constant k becomes an arc. Figure 9 re-plots all 2-D spectrograms of figure 8 using the

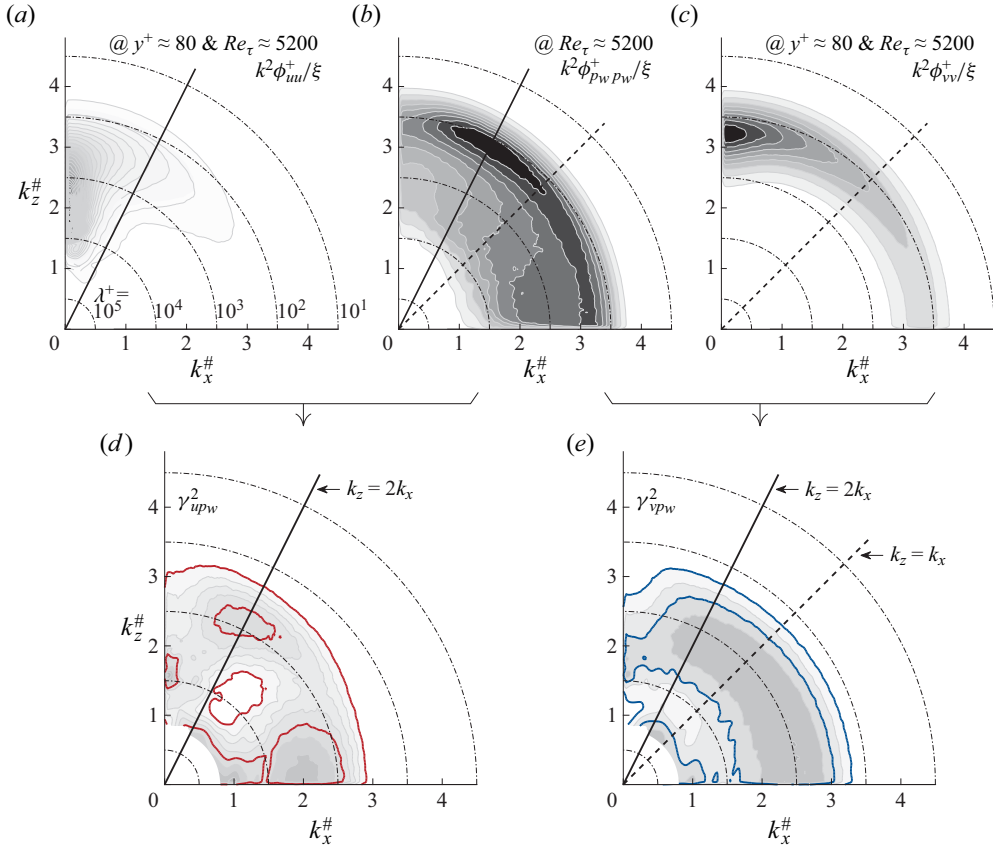


Figure 9. (a–c) Similar to figure 8(a–c) but now presented in log-polar format as described in the text; grey-scale contours show seven isocontours ranging up to the maximum value. (d,e) Similar to figure 8(d,e) but now presented in log-polar format. For indicating trends of scale isotropy, five dash-dotted arcs of constant $k = 2\pi/\lambda$ are plotted in all subfigures and correspond to $\lambda^+ = 10^1, 10^2, 10^3, 10^4$ and 10^5 (from the most outer arc going inward).

log-polar format, with $k_{ref}^+ = 1/50\,000$. Five arcs of constant $k = 2\pi/\lambda$ indicating the trend of scale isotropy are visualized with the dash-dotted lines on all plots and correspond to $\lambda^+ = 10^1, 10^2, 10^3, 10^4$ and 10^5 from the largest to the smallest arc. Lines of constant k_z/k_x correspond to the $k_z = 2k_x$ trend (solid line) and $k_z = k_x$ trend (dashed line).

For a detailed interpretation of the 2-D energy spectrograms of u and v in log-polar format (figure 9a,c), we refer to Lee & Moser (2019). From the wall-pressure spectrogram (figure 9b) it becomes evident that a significant part of the energy is distributed close to isotropically in scale, with a ridge at $\lambda^+ \approx 200$. The peak energy resides close to $\lambda_x = 2\lambda_z$, meaning that the pressure modes are, statistically, slightly elongated in the streamwise direction. Larger-scale energy (e.g. around the arc of $\lambda^+ = 10^3$) tends to be concentrated towards the $k_x^{\#}$ axis and, thus, resides in Fourier modes with k_z/k_x lower than 1 (or λ_x/λ_z lower than 1). When bringing in the coherence, for the wall pressure with v in figure 9(e), it peaks with a trend of scale isotropy around the $\lambda^+ = 10^3$ arc for $p_w v$ structures that are not strongly elongated in the streamwise direction (residing at $k_z < 2k_x$); contrary, the energy in v is relatively low at these large scales (figure 9c). Because the coherence is relatively strong below the $k_z = k_x$ line (in fact, constant at vector wavenumbers with

the same magnitude), while it weakens beyond $k_z \gtrsim 2k_x$, the following can be concluded. Fluctuations in v that are elongated in the spanwise direction z (residing at $k_z \lesssim k_x$) are energetically weak (see figure 9c) but are coupled to the wall-pressure imprint more strongly than v motions that are strongly elongated in x (residing at $k_z \gtrsim 2k_x$). The former would represent coherent spanwise vorticity, while the latter is representative of coherent streamwise vorticity. Concerning the u motions, $\gamma_{up_w}^2$ and the wall-pressure energy peak for streamwise elongated scales, along $k_z = 2k_x$. The scale at which the coherence peaks is larger since only the larger scales are coherent. Note that the single wall-normal position considered here is near $y^+ = 80$ and does not provide a full view: lower positions cause the peak coherence to reside at smaller scales (as was already observed in the 1-D analysis, see figure 6a). Hence, it will be beneficial to consider the scaling of coherence with y and Re_τ , before drawing further conclusions.

To present the 2-D coherence for p_w and u as a function of y and Re_τ , we reside to a representation based on distance-from-the-wall scaling. First, all cases of Re_τ are shown for a height of $y^+ \approx 80$ in figure 10(c); the darkest red contour re-shows the contour of figure 9(d) for $Re_\tau \approx 5200$. Here the axes of the log-polar format are adapted to account for the wall scaling: instead of $k_{ref}^+ = 1/50\,000$, the reference wavenumber is now made y dependent following $k_{yref} = 1/(1000y)$. This reference wavenumber is used in the new definition of the log-polar axes, $k_x^* = \xi k_x/k$ and $k_z^* = \xi k_z/k$, with $\xi = \log_{10}(k/k_{yref})$. Using the same format, two other wall-normal positions of $y^+ \approx 20$ (figure 10a) and $y^+ \approx 320$ (figure 10e) are considered. Alongside, the 2-D coherence for p_w and v is shown in the exact same format. All plots include six arcs of constant ky (or constant λ/y with the values stated in the caption), indicating trends of scale isotropy. Lines of constant k_z/k_x still correspond to those shown in figure 8, and indicate the $k_z = 2k_x$ trend (solid lines in figure 10a–f) and $k_z = k_x$ trend (dashed lines in figure 10b,d,f).

Isocontours of $\gamma_{up_w}^2$ in figure 10(a,c,e) collapse well for all Re_τ , in particular for the $\gamma_{up_w}^2 = 0.05$ isocontour. These plots reveal a wall scaling of the 2-D coherence because the isocontours appear at the same position for all three y positions, increasing consecutively by a factor of four ($y^+ \approx 20 \rightarrow 80 \rightarrow 320$). Note that isocontours are less well bundled at $y^+ \approx 320$; this is ascribed to only the very large (less-converged) scales being coherent. Figure 10(b,d,f) presents isocontours of coherence for p_w and v , and reveals a Reynolds-number-invariant wall scaling at the small-wavelength end. In contrast to u , the v isocontours of coherence adhere to trends of scale isotropy for $p_w v$ structures that are not strongly elongated in x (e.g. for scales residing at $k_z \lesssim 2k_x$). A maximum of the coherence resides near $\lambda/y = 8$ and is largely invariant with increasing λ_x/λ_z , except that the coherence shows a significant drop in amplitude for strongly stretched structures in x (this is more visible in figure 9f). Finally, the wall pressure is correlated stronger with v than with u ($\gamma_{vp_w}^2 > \gamma_{up_w}^2$).

As for the 1-D analysis in § 3.1, the 2-D coherence analysis is here extended to the coherence between the u and v motions and the wall-pressure squared. Contours of $\gamma_{up_w}^2$ and $\gamma_{vp_w}^2$ are shown in figures 11(a,c,e) and 11(b,d,f), respectively, and in a format identical to figure 10. Coherence $\gamma_{up_w}^2$ does not obey a perfect wall scaling, but for $y^+ \approx 80$ and $y^+ \approx 320$, the contours nearly collapse for all Re_τ and appear at similar locations in the plots. In general, the coherence with the wall-pressure-squared term resides at larger scales than the linear wall-pressure term, as was also the case in the 1-D analysis. Again, isocontours at the highest y position correspond to much larger scales with less smooth

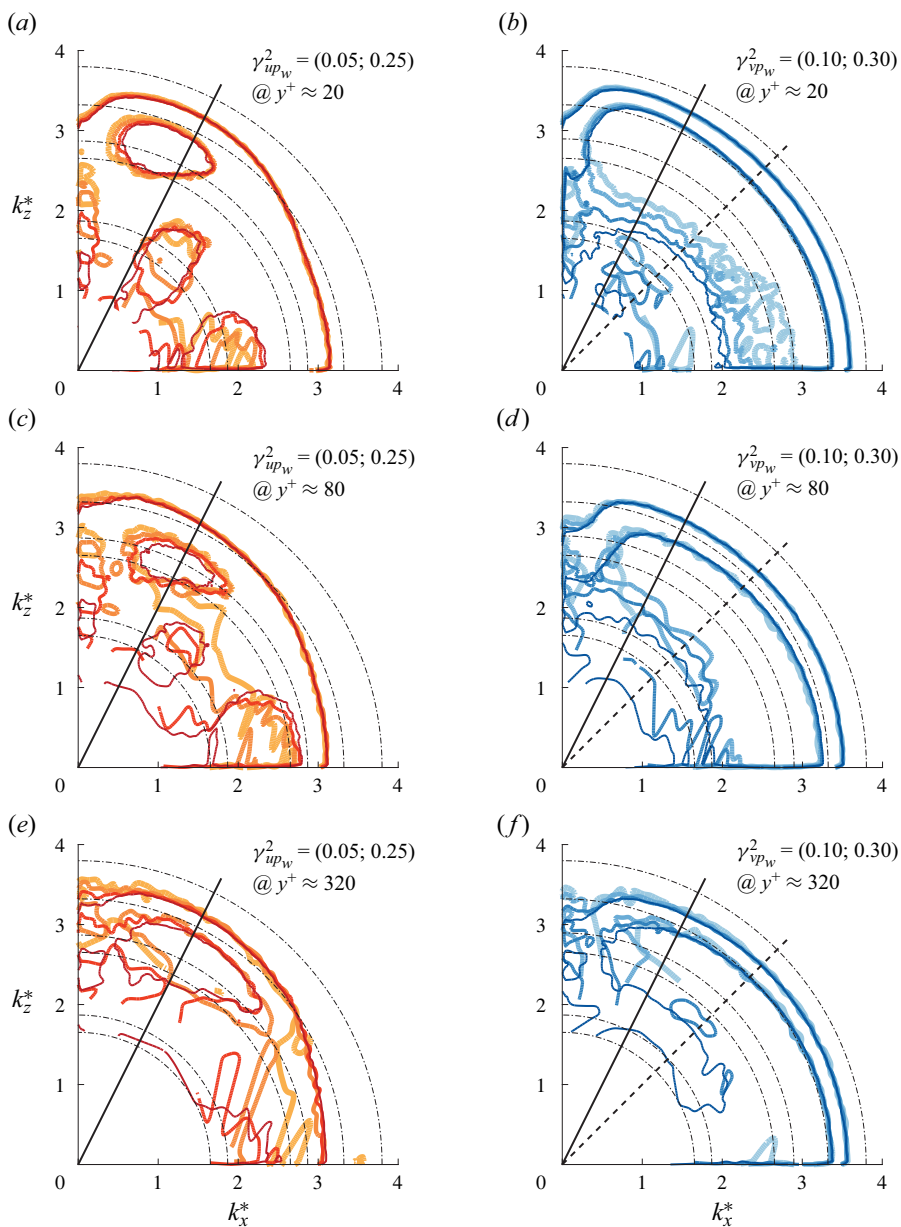


Figure 10. (a,c,e) Two-dimensional linear coherence of u and p_w , for all Re_τ cases and for three different inner-scaled wall-normal positions. Note that the wavenumber representation on the axes includes a wall scaling with y . The solid, coloured isocontours correspond to the same two contour values as were considered in figure 9(d), $\gamma_{up_w}^2 = [0.05; 0.25]$. (b,d,f) Similar to subfigure (a) but now for v and p_w , with the solid, coloured isocontours corresponding to the same two contour values as were considered in figure 9(e). For indicating trends of scale isotropy, dash-dotted arcs correspond to constant values of $\lambda/y = 1, 3, 8, 14, 85$ and 140 (from the most outer arc going inward).

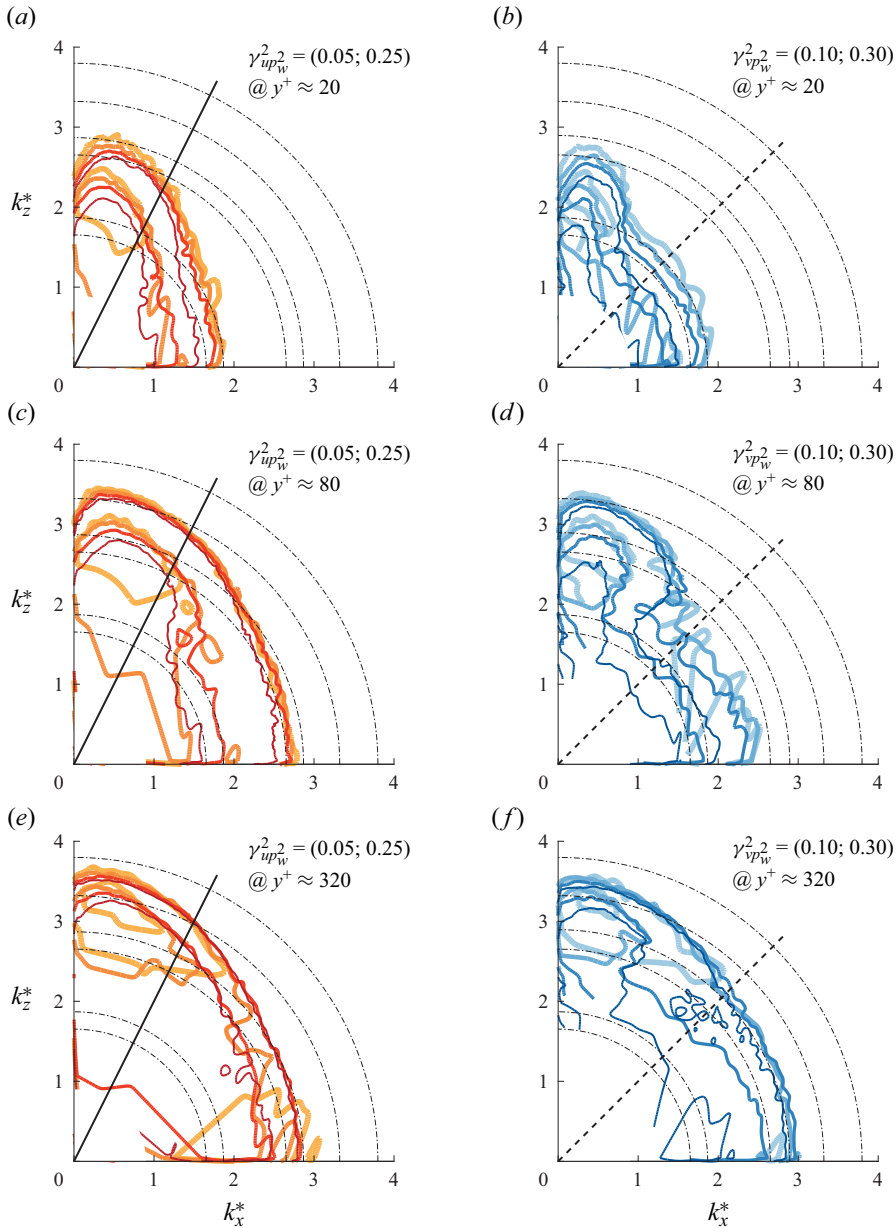


Figure 11. Similar to figure 10 but now for (a,c,e) u and p_w^2 (wall-pressure squared) and (b,d,f) v and p_w^2 .

spectral statistics, and for the two lowest Reynolds numbers, this position is beyond the logarithmic region. In the buffer region (at $y^+ \approx 20$ in figure 11a), the coherence remains nearly Reynolds-number invariant and no longer abides by a wall scaling. This was also apparent from figure 7(a). For the coherence of the wall-pressure-squared term with the v motions, observations are similar.

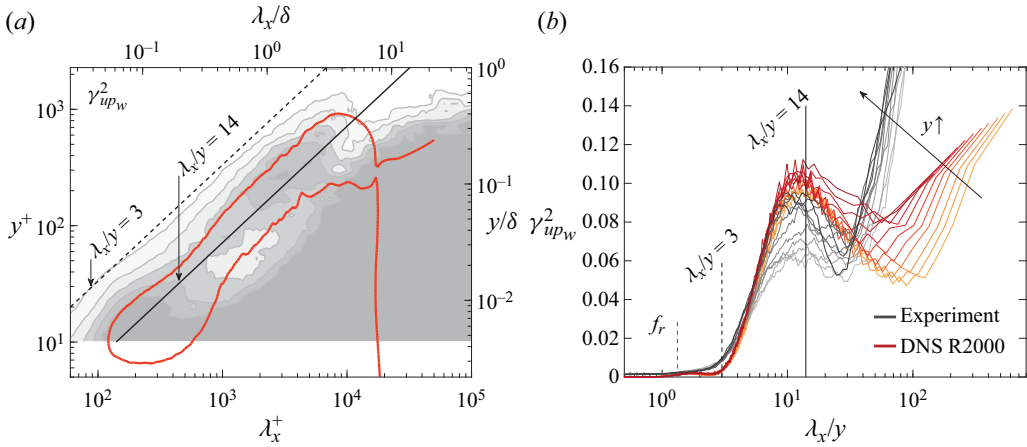


Figure 12. (a) Linear coherence spectrogram of u and p_w , for the experimental data (grey-scale filled isocontours 0.02:0.02:0.1) and DNS R2000 data (a single red contour at $\gamma_{up_w}^2 = 0.08$). (b) Linear coherence spectra for 11 positions within the logarithmic region, in the range $80 \lesssim y^+ \lesssim 0.15Re_\tau$. Results in frequency space are converted to a wavelength dependence using $\lambda_x \equiv \bar{U}(y)/f$.

4. Exploring velocity-state estimation using sparse experimental data

Now that Reynolds-number scalings of the wall-pressure–velocity were identified, experimental wall pressure and velocity data are assessed for exploring whether velocity-state estimation based on wall-pressure input data is feasible (in practice). At first, the experimental findings are compared with the DNS-inferred correlations in § 4.1, after which the quadratic stochastic approach for velocity-state estimation is outlined in § 4.2. Finally, in § 4.3 the accuracy in the velocity-state estimates is discussed.

4.1. Coherence of single-point input–output data

With the available experimental time series of the streamwise velocity, $u(y, t)$, and the corresponding post-processed wall pressure $p_w(t)$, the linear coherence $\gamma_{up_w}^2$ is computed in frequency space. Note that we only consider the wall-pressure–velocity correlation with the u component since the single hot-wire probe measurements performed only provide streamwise velocity time series. Figure 12(a) shows the coherence spectrogram after conversion from a frequency-to-wavelength dependence, using the local mean velocity (§ 2.2). Overlaid is one isocontour computed from the DNS R2000 data, highlighting that the ridge of strong coherence was well captured by the experiment. Inspection of the slightly noisier experimental spectrogram is facilitated by showing individual coherence spectra in figure 12(b), for 11 positions within the logarithmic region taken as $80 \lesssim y^+ \lesssim 0.15Re_\tau$. Seemingly, the experimental spectra agree well in terms of the onset of coherence at a wall scaling of around $\lambda_x/y = 3$ and its peak residing near $\lambda_x/y = 14$. For lower y positions (a lower grey-scale intensity), the peak magnitude is underestimated compared with the DNS-inferred value of $\gamma_{up_w}^2|_{\text{peak}} \approx 0.1$. A lower coherence is expected, given that denoising of experimental data is never perfect and, thus, leaves (incoherent) energy within the $p_w(t)$ signals.

A primary difference between the DNS and experimental coherence is observed for very large wavelengths. While coherence for the DNS increases beyond a constant $\lambda_x \approx 10\delta$ for all y , the experimental coherence shows a kick-up around $\lambda_x/y \approx 30$. We conjecture

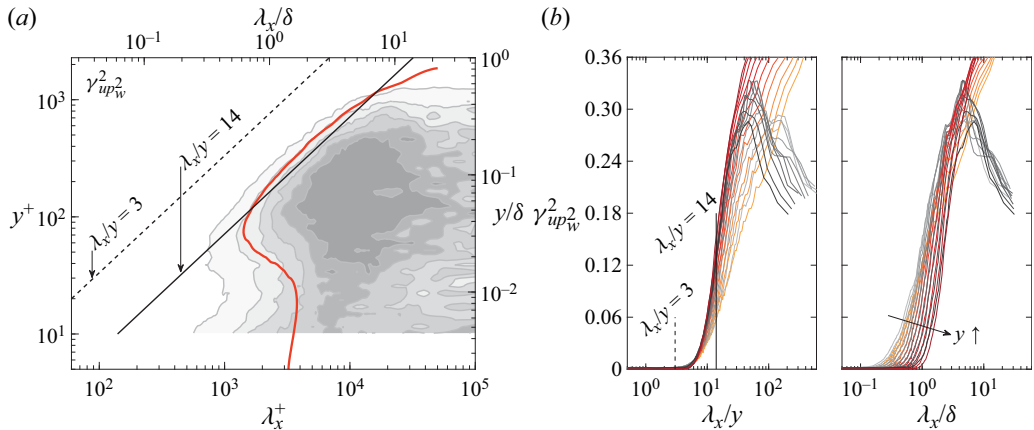


Figure 13. (a) Linear coherence spectrogram of u and p_w^2 , for the experimental data (grey-scale filled isocontours 0.04:0.04:0.24) and DNS R2000 data (a single red contour at $\gamma_{up_w^2}^2 = 0.08$). (b) Linear coherence spectra for 11 positions of the experimental data within the logarithmic region, in the range $80 \lesssim y^+ \lesssim 0.15Re_\tau$. Results in frequency space are converted to a wavelength dependence using $\lambda_x \equiv \bar{U}(y)/f$.

that the latter is related to the facility-noise filtering procedure of the experimental wall pressure (described in [Appendix A](#)). That is, the energy content at larger streamwise wavelengths is attenuated in comparison to the DNS (see [figure 20b](#) in [Appendix A](#)). This attenuated energy resides at relatively large spanwise scales of $\lambda_z > 1.8\delta$, and these scales of the wall-pressure field are generally less coherent with the grazing velocity fluctuations. Hence, the retained energy in the noise-filtered experimental pressure data is relatively more coherent. Nevertheless, this section illustrates that with the adopted filtering procedures, the experiment is able to capture the general characteristics of the wall-pressure–velocity coupling. According to the authors’ knowledge, this has not been attempted before and, hence, is an important result for the practical implementation of wall-pressure-based control.

For the nonlinear pressure coherence, $\gamma_{up_w^2}^2$, the comparison between the experiment and DNS is presented in [figure 13](#) in a similar way as for the linear coherence in [figure 12](#). Within the logarithmic region, the onset of coherence beyond $\lambda_x/y = 14$ is well captured. A slight discrepancy in the near-wall region between the experimental and DNS isocontours of $\gamma_{up_w^2}^2 = 0.08$ is ascribed to the difference in spatial and temporal coherence spectra. Recall the discussion of [figure 7](#) in that the coherence involving p_w^2 relates to an intensity modulation in which pressure fluctuations become more/less intense at a spatial scale that is a multiple of the dominant (linearly) correlated scale.

4.2. Stochastic estimation

For a real-time controller working with wall-based sensing, a state estimation of the turbulence velocity fluctuations is critical. An overview of LSE and QSE was provided in [§ 1.1](#), and these are here implemented in the time domain to illustrate the state estimation and quantify the estimation accuracy. Stochastic estimation procedures are performed in frequency space (not wavelength space) since the experimental data comprise time series. When concentrating on LSE, the time-domain estimate of the logarithmic region u

fluctuations at y_e can be formed through the convolution

$$\hat{u}_{LSE}(y_e, t) = (h_l \otimes p_w)(t), \quad (4.1)$$

where the temporal kernel is the inverse Fourier transform of the frequency-domain kernel, $h_l = \mathcal{F}^{-1}[H_L]$, with

$$H_L(y_e, f) = \frac{\phi_{up_w}(y_e; f)}{\phi_{p_w p_w}(f)} = |H_L(f)| e^{j\psi(y_e; f)}. \quad (4.2)$$

The expression (4.2) is equivalent to (1.4), but for a 1-D frequency dependence, and the kernel's gain can be related to the coherence, according to

$$|H_L(y_e; f)| = \sqrt{\frac{\gamma_{up_w}^2(y_e; f) \phi_{uu}(y_e; f)}{\phi_{p_w p_w}(f)}}. \quad (4.3)$$

For QSE, the time-domain estimate can be written as the first higher-order term of the input pressure p_w (Naguib *et al.* 2001):

$$\hat{u}_{QSE}(y_e, t) = (h_l \otimes p_w)(t) + (h_q \otimes p_w^2)(t). \quad (4.4)$$

As noted in § 1.1, when the probability density function (PDF) of the input is symmetric, the linear kernel in the QSE is equal to the one in the LSE (for our experimental wall-pressure data the skewness is negligible, see figure 21 in Appendix A). The quadratic kernel also follows from the inverse Fourier transform of the frequency-domain kernel, $h_q = \mathcal{F}^{-1}[H_Q]$, with

$$H_Q(y_e, f) = \frac{\phi_{up_w^2}(y_e; f)}{\phi_{p_w^2 p_w^2}(f)}. \quad (4.5)$$

For completeness, the linear and quadratic kernels can also be written just in terms of the two-point correlations:

$$h_l(y_e, \tau) = \frac{\langle p_w(t) u(y_e, t + \tau) \rangle}{\langle p_w^2 \rangle}, \quad h_q(y_e, \tau) = \frac{\langle p_w^2(t) u(y_e, t + \tau) \rangle}{\langle p_w^2 \rangle^2}. \quad (4.6a, b)$$

Estimates are now performed, for which transfer kernels were first generated from 50 % of the available data (thus from time series of $T_a/2$ long, still spanning more than 16 000 boundary layer turnover times). The remaining time series data were used for the estimation. Results for an unconditional estimate of the u fluctuations at $y_e^+ \approx 80$ are shown in figure 14(a). Time series are shown for a total duration of $\Delta t^+ = 3000$, based on the LSE and QSE. Estimates are compared with the true (measured) time series: the raw measured time series is shown with the grey line, while a large-scaled filtered version, u_W , is shown with the black line. This latter signal u_W only retains the wall-attached scales, which are defined as the streamwise velocity fluctuations that are correlated with the wall-shear stress (or friction velocity) fluctuations. Practically, u_W is a large-scale pass-filtered signal of u , and the filter was derived from velocity–velocity correlations and was confirmed to be Reynolds-number invariant (Baars *et al.* 2017). This spectral filter has a definitive cutoff at $\lambda_x/y = 14$ and, thus, also comprises a wall scaling $\lambda_x \sim y$, meaning that only progressively larger scales are retained for larger y positions. Further details of this filter can be found in the literature (figure 9 and pp. 16–17 of Baars & Marusic 2020). Note that u_W will serve as a reference case for comparing the estimations to since the filtered fluctuations following a wall scaling are more representative of the fluctuations that can physically be estimated using stochastic estimation. When inspecting figure 14(a), it is evident that the QSE procedure better estimates u_W (and thus, also u), but this is further quantified in the next section.

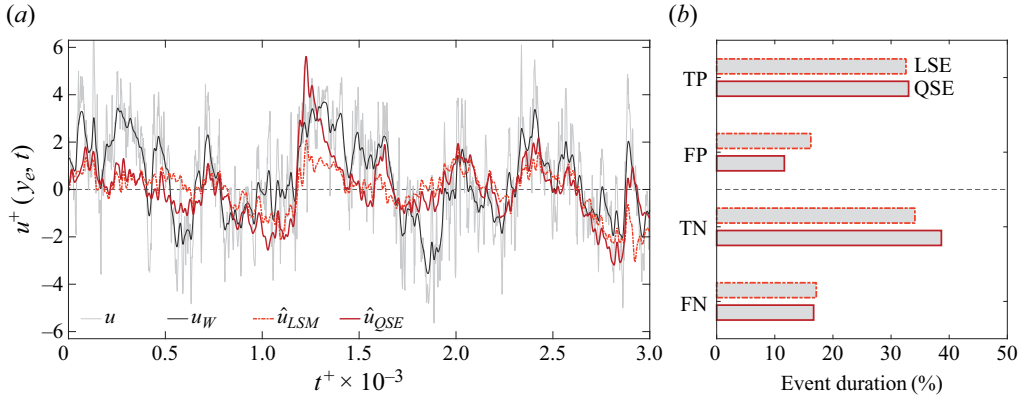


Figure 14. (a) Sample of the stochastic estimate of the u fluctuations at $y_e^+ \approx 80$, based on wall pressure, in comparison to a true (measured) time series. The measured hot-wire time series $u(y_e, t)$ is shown with a grey line, and is filtered to only retain the wall-attached u fluctuations, $u_W(y_e, t)$, shown with the black line. Estimates using LSE, $\hat{u}_{LSE}(y_e, t)$, and QSE, $\hat{u}_{QSE}(y_e, t)$, are shown with orange and red lines, respectively. Correlation coefficients of the measured wall-attached u fluctuations and the linear estimate (u_W with \hat{u}_{LSE}), and the quadratic estimate (u_W with \hat{u}_{QSE}), equal 0.48 and 0.60, respectively (see figure 15b for $y_e^+ \approx 80$). (b) Time percentage of binary events in the LSE (orange dash-dotted line) and QSE (red solid line), relative to u_W .

4.3. Accuracy of velocity-state estimation

We here assess the accuracy of the velocity-state estimates using a binary-state approach as well as a conventional correlation coefficient. When flow control systems would operate with on/off (binary) actuators only (Abbassi *et al.* 2017), actuators would, in its simplest form, operate based on the estimated signal's sign (e.g. with a zero-valued threshold). In this context, the goodness of the estimates is quantified with a binary accuracy (BACC). When binarizing u_W (here considered as the true signal) and the estimated signal (\hat{u}_{LSE} or \hat{u}_{QSE}) at every time instant, only four events are possible: a true positive (TP) occurs when both signals are positive, whereas both signals being negative will yield a true negative (TN). Additionally, false positive (FP) and false negative (FN) linear estimates occur for $u_W(t) < 0$ and $\hat{u}_{LSE}(t) \geq 0$, or *vice versa*, respectively. The BACC, defined as

$$\text{BACC} = \frac{T_{TP} + T_{TN}}{T}, \quad (4.7)$$

represents the cumulative time that the estimate is a true positive and negative ($T_{TP} + T_{TN}$), relative to the total duration of the signal. Note that a BACC of unity does not mean that the estimate is perfect (that would be $\hat{u}_{LSE}(t) = u_W(t)$), but only that $\text{sgn}[\hat{u}_{LSE}(t)] = \text{sgn}[u_W(t)] \forall t$. Figure 14(b) presents the time percentage of each of the four binary events for the full estimate of the case shown in figure 14(a). The total BACC for the LSE procedure is 66.7 %, while the QSE improves this to 71.7 %. This improvement comes from an increase of TN instances at the expense of less FP instances (such occasions appear around $t^+ \times 10^{-3} = 0.6$ and $t^+ \times 10^{-3} = 1.8$ in figure 14a).

To quantify the goodness of the estimate further, the BACC is plotted for a range of y_e , starting at the lower end of the logarithmic region, $y_e^+ \approx 80$, up to the start of the intermittent region at $y_e^+ = 0.4Re_\tau$. Figure 15(a) includes three profiles: the red ones are based on wall-pressure input, using both LSE and QSE, while the orange is based on an LSE with a representative wall-friction velocity input. This latter case considers data acquired in an identical experiment as the current one, except that the wall-pressure quantity was replaced with a single hot-film sensor on the wall, yielding a voltage signal as

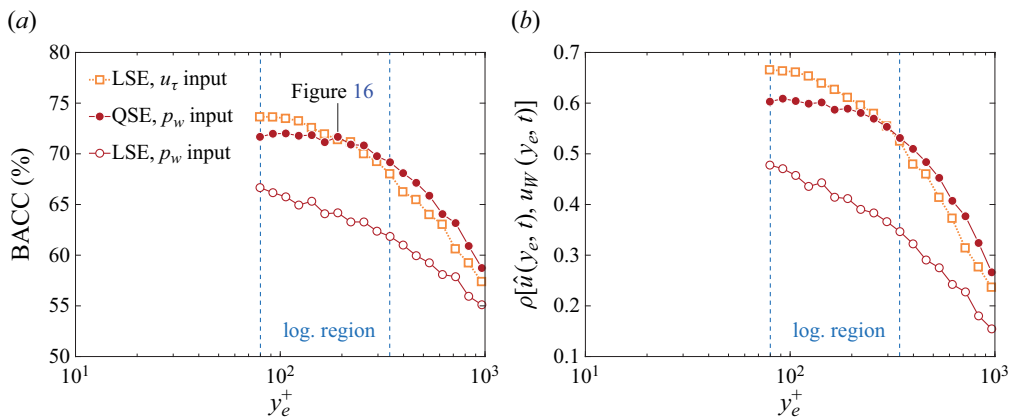


Figure 15. (a) The BACC for a range of estimation positions, y_e . (b) Similar to subfigure (a) but now for the correlation coefficient between the LSE- and QSE-based estimates and the true large scales, taken as u_W .

a surrogate for the fluctuations in friction velocity (see Abbassi *et al.* 2017; Dacome *et al.* 2023). It is well known that a hot film yields relatively clean signals (not subject to facility noise as is the wall pressure) and that the linear correlation between the wall signal and the off-the-wall velocity fluctuations is relatively strong (e.g. Hutchins *et al.* 2011; Baars *et al.* 2017). Note that it was confirmed that for this case with a friction velocity input, a QSE does not result in an improved estimate per the findings of Guezennec (1989). Finally, before interpreting the results, it is important to put the BACC magnitude into perspective. An estimate with a BACC of 50 % would reflect a random process and would thus be, on average, impractical when attempting real-time control based on such an estimate. In the real-time control work of Abbassi *et al.* (2017) it was shown that real-time control with a BACC level of around 70 % was sufficient for targeting specific structures (e.g. positive or negative excursions in streamwise velocity). They used a friction velocity input for their off-the-wall velocity-state estimation, and their case is represented by the ‘LSE, u_τ input’ curve in figure 15(a). Hence, this case serves as a (successful) reference case.

For an LSE procedure with wall-pressure input, the BACC in the logarithmic region remains below 67 %. However, a QSE procedure results in a very similar BACC (mostly in excess of 72 %) as the reference case with the LSE based on a hot-film sensor input. Hence, the current analysis shows that velocity-state estimation of the turbulent flow in the logarithmic region is viable with wall-based pressure sensing (provided that the quadratic pressure term is included), even when significant levels of facility noise are present.

Similar trends as for the BACC curves are found when concentrating on a conventional cross-correlation coefficient between the estimated signals and the true (large-scale) filtered signal u_W . Figure 15(b) presents profiles of the correlation coefficient of the measured wall-attached u fluctuations and the linear estimate (u_W with \hat{u}_{LSE}), and the quadratic estimate (u_W with \hat{u}_{QSE}). A correlation coefficient of u_W with a wall-friction velocity signal is also shown for reference. As for the observations made based on the BACC, the inclusion of the quadratic term of the wall pressure improves the correlation of the estimated signal with the true signal, u_W : the normalized correlation coefficient reaches 0.60 (at $y_e^+ = 80$) with the QSE, while the LSE only results in a correlation coefficient of 0.48. Thus, not only does the BACC show good promise for wall-based pressure sensing to perform off-the-wall velocity estimates, but further details of the velocity fluctuations themselves – as captured by a correlation coefficient – are also

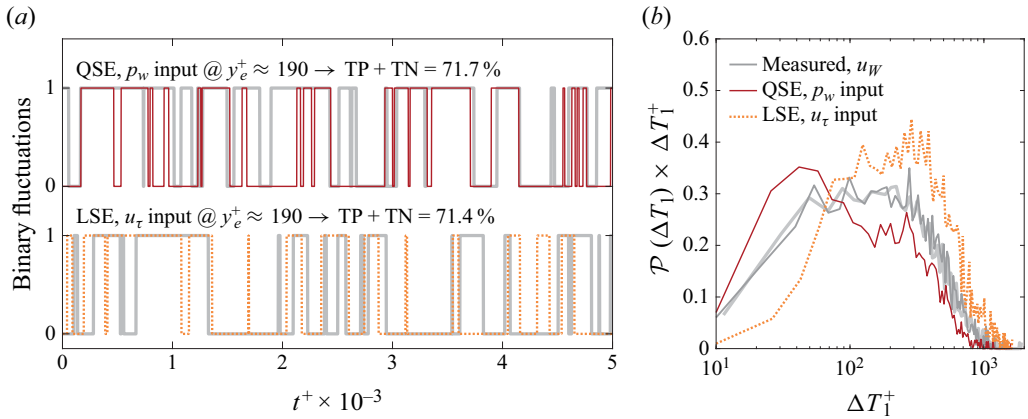


Figure 16. (a) Binary fluctuations of the QSE in solid dark red (top row) and LSE in dashed orange (bottom row) near the geometric centre of the logarithmic region, compared with the binary fluctuations of the true large scales, u_W , in grey. (b) Premultiplied PDFs of all uninterrupted time spans for which the binary signals equal unity (ΔT_1).

well captured. In this regard, a final comparison between the binary fluctuations obtained through QSE with the wall pressure, and LSE with the hot-film sensor input is made in figure 16. Near the geometric centre of the logarithmic region, at $y_e^+ \approx 190$, the BACC and correlation coefficient are nearly identical (see figure 15a,b). Binary fluctuations of the estimates, as well as the true large-scale signal u_W are shown in figure 16(a). Note that these two sets of time series are not synchronized, since they come from different experiments. Differences in the estimations are summarized in terms of a PDF of all uninterrupted time spans for which the binary signals equal unity (denoted as time span ΔT_1). This PDF is presented in premultiplied form (figure 16b), so that longer time spans are weighted accordingly, e.g. the area under the curve is representative of how much a range of ΔT_1 contributes to the total time series duration. The PDFs corresponding to the true signals (the two grey binary fluctuations on the left) are equal as expected. Even though the BACC is equal for the two estimates, the binary fluctuations obtained with QSE (p_w input) results in more ‘short’ events, while the LSE (u_τ input) results in more ‘long’ events (cross-over at $\Delta T_1^+ \approx 100$). So although the current findings show the feasibility of velocity-state estimation based on wall-pressure sensing, further research should address this accuracy in more detail by considering temporal-accuracy characteristics, its application in real-time control and robustness to actuator noise and other external sources of noise.

5. Concluding remarks

This work has been motivated by the potential feasibility of using wall-pressure input data for estimating off-the-wall turbulent velocities. Such an estimation capability is of high interest to realizing real-time controllers for wall-bounded turbulence – solely relying on wall-pressure input data – as long as they have a sufficient velocity-state estimation capability and are robust with variations in Reynolds number. The latter requires a firm understanding of the Reynolds-number scaling of wall-pressure–velocity correlations. In this regard, we examined the scaling behaviour of the coherence between the turbulent velocity fluctuations and the wall-pressure field, based on DNS data of turbulent channel

flow with a Reynolds-number range $Re_\tau \approx 550\text{--}5200$. Several findings are summarized as follows.

- (i) Not only the 1-D coherence analysis (§ 3.1) but also a 2-D coherence analysis (§ 3.2) revealed that the coherence between p_w and u , and p_w and v , adhere to a Reynolds-number-invariant wall scaling with y .
- (ii) A 1-D streamwise data analysis with u and v velocity fluctuations at a given y position revealed that they are most strongly coupled to the linear term of the wall-pressure fluctuations, p_w , at a scale of $\lambda_x/y \approx 14$ and $\lambda_x/y \approx 8$, respectively.
- (iii) With the 2-D extension of the analysis as a function of λ_x and λ_z , it was shown that the peak coherence for p_w and u remains near $\lambda_x/y \approx 14$ and is reasonably symmetric around $\lambda_x/\lambda_z = 2$. The 2-D coherence for p_w and v peaks around $\lambda_x/\lambda_z = 1.0$.
- (iv) When statistically combining the results from the 1-D and 2-D analyses, it can be concluded that the ridge of coherence for p_w and u scales following $\lambda_x : \lambda_z : y \propto 14 : 7 : 1$, while for p_w and v , the scaling is $\lambda_x : \lambda_z : y \propto 8 : 8 : 1.0$.
- (v) Based on the 2-D analysis, turbulent motions in v that are coherent with p_w show a much stronger isotropic behaviour than the u motions, and also possess a higher coherence magnitude. While the u motions elongated in x following $\lambda_x/\lambda_z \approx 2$ are most coherent, the v motions that are most coherent reside near a 2-D wavevector of $\lambda/y = 8$ and is largely invariant with increasing λ_x/λ_z up to only very strongly stretched structures in x beyond $\lambda_x \gtrsim 3\lambda_z$.
- (vi) The coherence with the wall-pressure-squared term p_w^2 resides at larger scales than the linear wall-pressure term, as was also the case in the 1-D analysis. The coherence involving p_w^2 is reminiscent of a (large-scale) intensity modulation of the pressure fluctuations. This is because the coherence dominates at a spatial scale that is a multitude of the characteristic (linearly correlated) fluctuations and because the coherence with the quadratic term, p_w^2 , is strongest for the velocity fluctuations taken in the logarithmic region. The latter reflects the general consensus that the modulation of wall quantities is driven by energetic large-scale motions in the logarithmic region of the flow.

With the DNS data spanning a decade in friction Reynolds number and the appearance of a clear Reynolds-number invariance when adopting a wall scaling $\lambda_x \sim y$, the current work suggests strong evidence that an extrapolation of the scaling laws to higher Re_τ conditions can be made. Moreover, an experimental dataset comprising simultaneous measurements of wall pressure and velocity provided ample evidence, at one value of $Re_\tau \approx 2k$, that the DNS-inferred correlations can be replicated with experimental pressure data subject to significant levels of (acoustic) facility noise. It was furthermore shown that in order to reach similar levels of estimation accuracy in the wall-pressure-based estimates, compared with estimates based on an input resembling friction velocity fluctuations, it is critical to include the quadratic pressure term. This is consistent with earlier observations of Naguib *et al.* (2001) who explored a time-domain QSE for the estimates of the conditional streamwise velocity. An accuracy of up to 72 % in the binary state of the streamwise velocity fluctuations in the logarithmic region is achieved; this corresponds to a correlation coefficient of ~ 0.6 . Since measuring the fluctuating wall pressure is relatively robust in practice and is a viable quantity to measure on an aircraft fuselage, the current study is a step towards the implementation of a reliable flow state estimation framework for wall-bounded turbulence based on wall pressure.

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Appendix A. Post processing of the experimental wall-pressure signals

Wall-pressure measurements with microphones, surface embedded behind pinholes, require several post-processing steps to yield valid time series of the fluctuating wall pressure. Background noise is well known to contaminate pressure measurements in wall-bounded turbulence, particularly at relatively low Re_τ when the facility noise can overshadow the turbulence-induced pressure fluctuations. For instance, Klewicki *et al.* (2008) compiled an empirical relation for the inner-scaled wall-pressure intensity, as a function of Re_τ ,

$$p_w'^+ = \frac{p_w'}{\tau_w} = \sqrt{6.5 + 2.30 \ln \left(\frac{Re_\tau}{333} \right)}. \quad (A1)$$

According to this formulation, the expected wall-pressure intensity in the W-tunnel facility is $p_w' \approx 1.13$ Pa (with parameters of table 1). This equates to an overall sound pressure level of roughly 95 dB ($p_{ref} = 20$ μ Pa). For the non-anechoic facility, the noise level exceeds this value. That is, the acoustic pressure intensity in the potential flow was measured to be 105 dB, revealing the clear need for the implementation of a noise cancelling scheme. In total, three corrections were implemented: step 1 uses the spanwise extent of the wall-pressure array (a unique feature of the current study), whereas steps 2 and 3 are conceptually similar to the procedure described in Appendix A of Tsuji *et al.* (2007) and Gibeau & Ghaemi (2021). These steps convert the measurement time series of the centre pinhole-mounted microphone (further denoted as $p_{w1} = p_4$) to a corrected wall-pressure signal: $p_{w1} \rightarrow p_{w2} \rightarrow p_{w3} \rightarrow p_{w4}$. Representative positions corresponding to the first three signals are shown in figure 19(d).

Step 1: Subtract spanwise mean. The spanwise array with $S = 7$ pinhole-mounted microphones spanned a total width of $\Delta z = 1.78\delta$, thus resolving spanwise wavelengths up to $\lambda_z \approx 1.8\delta$ (see figure 17a). Note that the details of the sensors themselves (GRAS 46BE $\frac{1}{4}$ in. microphones) and the pinhole-mounted microphone arrangement were described in § 2.2. At each temporal instant t_i , all energy in the pressure fluctuations residing at spanwise wavelengths $\lambda_z > 1.8\delta$ is provided by the spanwise-mean pressure,

$$p_{span}(t_i) = \frac{1}{S} \sum_{s=1}^S p_s(t_i). \quad (A2)$$

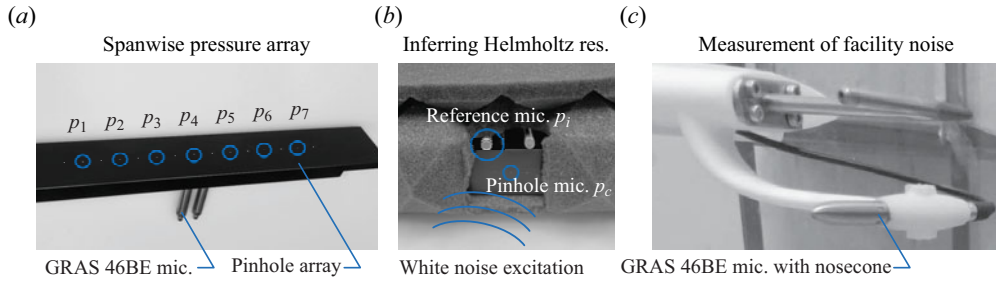


Figure 17. (a–c) Experimental hardware used to measure wall-pressure fluctuations in the W-tunnel facility.

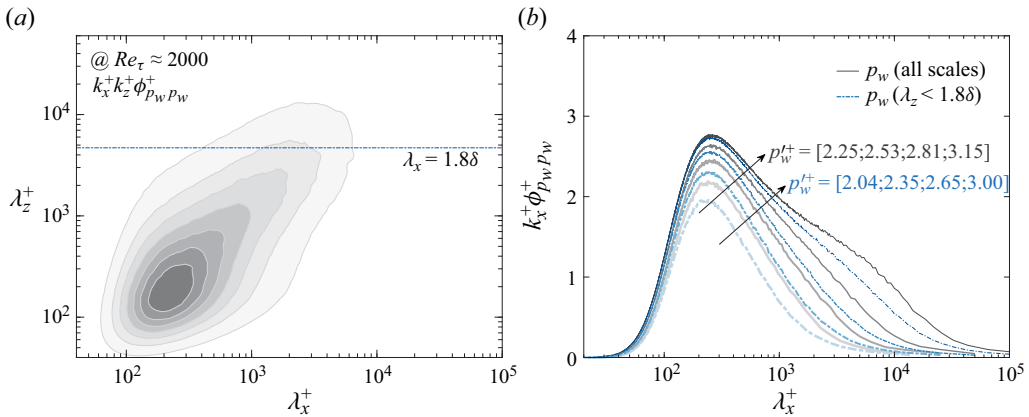


Figure 18. (a) Two-dimensional spectrogram of p_w for the R2000 DNS case. (b) One-dimensional wall-pressure spectra, constructed from the integration of the 2-D spectra with the full range of spanwise scales (grey lines) and the spanwise scales limited to $\lambda_z < 1.8\delta$ (blue lines).

When subtracting this time series from measurement p_{w1} , a filtered signal follows,

$$p_{w2}(t) = p_{w1}(t) - p_{span}(t), \quad (\text{A3})$$

and still corresponds to the position of the microphone diaphragm. Even though (A3) can be considered a conventional subtraction-based method (as opposed to an optimal filtering scheme, e.g. Naguib, Gravante & Wark 1996), the current scheme relies on the spanwise width and convergence of a seven-point mean. That is, all removed energy at $\lambda_z > 1.8\delta$ can only come from (1) the large-scale turbulence-induced wall pressure and/or (2) acoustic noise of the facility. Ideally, the latter is removed while the former is preserved. In order to assess how much energy of turbulence-induced pressure fluctuations resides at those scales, the DNS data are used. A 2-D wall-pressure spectrum at $Re_\tau \approx 2000$ is shown in figure 18(a), together with the spanwise cutoff wavelength of the pressure array. When integrating over λ_z , the 1-D streamwise spectrum is obtained and shown in figure 18(b). In fact, two sets of spectra are shown: the raw 1-D spectra and those that exclude the energy at $\lambda_z > 1.8\delta$ for all four Reynolds numbers (but note that only the R2000 case is relevant for the current experiments at closely matched Re_τ). It is evident that only a small degree of large-scale energy is removed by subtracting the spanwise-mean pressure over the array, as evidenced by the integrated wall-pressure intensities listed in the annotations. For the R2000 case, the difference in integrated spectral energy is $\approx 6\%$.

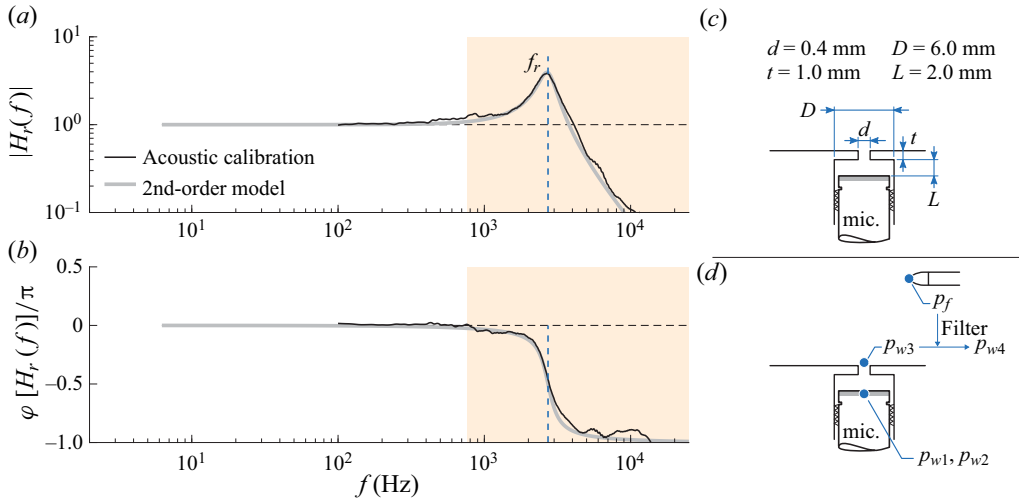


Figure 19. (a,b) Gain and phase of the resonator's transfer kernel. A comparison is made between the kernel obtained from the acoustic calibration and a model kernel fitted to these empirical results. The filled area indicates the frequency range at which there is no expected coherence for the current study (further described in the text). (b) Geometric parameters of the pinhole-mounted microphone arrangement. (c) Wall-pressure signals that are being considered in the post-processing sequence.

Since facility noise generally propagates as plane waves, acoustic noise reaches all microphones at equal times. Hence, subtraction of the spanwise mean through (A3) is an effective denoising procedure as seen from the spectra of the raw (p_{w1}) and spanwise-filtered (p_{w2}) pressure signals in figure 20(a).

Step 2: Helmholtz correction. A pinhole configuration to enhance the spatial resolution of the microphone results in an unavoidable sub-surface cavity above the diaphragm, and thus, Helmholtz resonance. Resonance amplifies the measured cavity pressure, relative to the excitation signal at the pinhole inlet, at frequencies close to resonance. When sizing the resonator, the design resonance frequency, f_0 , was computed from the formulation (Ingard 1953; Panton & Miller 1975),

$$f_0 = \frac{a_0}{2\pi} \sqrt{\frac{S}{V(t + t^*) + L^2 S/3}}, \quad (\text{A4})$$

where a_0 is the speed of sound, $S = \pi d_0^2/4$ is the area of the orifice, $V = \pi D^2 L/4$ is the cavity volume and t^* is an 'end correction'. This correction is required, as besides the air within the neck, a small portion of air inside the cavity and outside of the orifice will displace as well. When taking the end correction from Ingard (1953), $t^* = 0.48\sqrt{S}(1 - 1.25d_0/D)$ and is valid for $d_0/D < 0.4$ only, the design resonance frequency becomes $f_0 = 2725$ Hz (dimensions of the pinhole and cavity are shown in figure 19c). Amplification of energy surrounding the resonance frequency is apparent from the broadband hump in the spectrum of p_{w2} in figure 20(a).

Correcting for the Helmholtz resonance is straightforward once the resonator has been characterized. Whereas (A4) provides a design frequency f_0 , it does not consider how the amplitude and phase of the measured pressure in the cavity relates to the inlet pressure. This can be modelled through a single input/output impulse transfer function, $H_r(f)$, by considering the mass-spring-damper system equivalent of the resonator. Its gain and phase

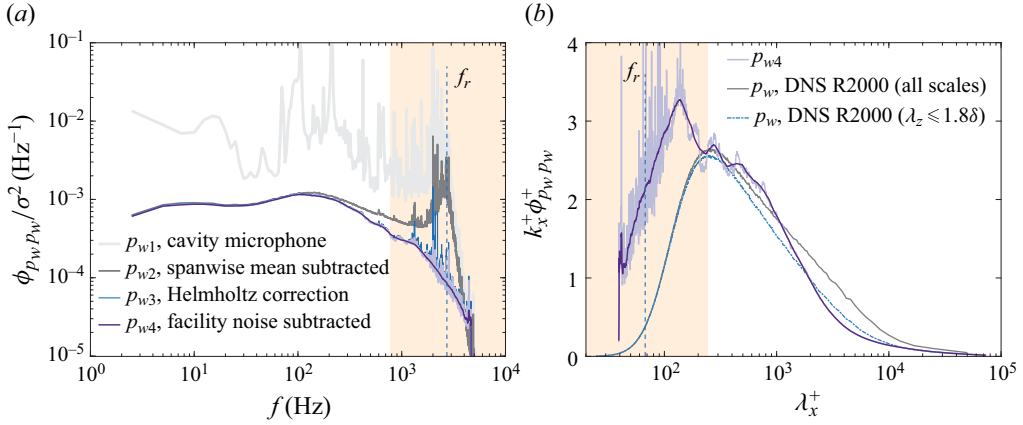


Figure 20. (a) Spectra of the various wall-pressure signals generated in the post-processing procedure. (b) Spectrum of the final, corrected wall-pressure signal obtained from experiments, compared with the spatial wall-pressure spectra from DNS.

are formulated as

$$|H_r(f)| = \left[\left(1 - \left(\frac{f}{f_r} \right)^2 \right)^2 + \left(\frac{2\xi f}{f_r} \right)^2 \right]^{-0.5} \quad \text{and} \quad \varphi[H_r(f)] = -\tan^{-1} \left[\frac{2\xi(f/f_r)}{1 - (f/f_r)^2} \right]. \quad (\text{A5a,b})$$

Here, ξ is a damping constant and f_r is the resonance frequency. Both ξ and f_0 require empirical characterization through a calibration experiment, using acoustic pressure excitation. This experiment was conducted in a facility that is anechoic at frequencies above 200 Hz (Merino-Martínez *et al.* 2020). White noise was produced with a Bose[®] speaker and was recorded simultaneously by a reference microphone (measuring the excitation pressure at the inlet, p_i) and the cavity microphone (p_c); see figure 17(b). Signals were acquired for a length of $T_a = 150$ s at a sample rate of $f_s = 51.2$ kHz. With the signal recordings, the experimental characterization of the Helmholtz resonator can be obtained through dividing the input–output cross-spectrum by the input spectrum:

$$|H_r^{exp}| = \frac{\langle P_c(f) P_i(f) \rangle}{\langle P_i(f) P_i^*(f) \rangle}. \quad (\text{A6})$$

Ensemble averaging was conducted using FFT partitions of $N = 2^{13}$ samples, resulting in a spectral resolution of $df = 6.25$ Hz and 1870 ensembles with 50 % overlap. The resultant gain and phase of the complex-valued kernel are plotted in figure 19(a,b), but only for $f > 100$ Hz due to the non-anechoic nature of the facility at lower frequencies, causing non-physical behaviour. The second-order model transfer function $H_r(f)$ was fit to the data to infer the resonance frequency and damping coefficient, yielding $f_r = 2725$ Hz and $\xi = 0.128$, respectively. The measured kernel captures the experimental behaviour well, and the resonance frequency closely resembles the design frequency ($f_r/f_0 \approx 0.99$). The gain function shows the region of amplification around f_r , and the resonance peak is associated with the well-known phase reversal between the excitation signal and cavity response.

Note that the time series of pressure at the pinhole inlet can be generated by a convolution of the cavity pressure signal with the time-domain transfer kernel,

$$p_{w3}(t) = (h_r^{exp} \circledast p_{w2})(t). \quad (\text{A7})$$

Here $h_r^{exp} = \mathcal{F}^{-1}[H_r^{exp}]$ is taken from the experimental characterization. Before proceeding, it is important to provide a note on the frequency range of interest. To utilize the wall pressure for estimating the state of the off-the-wall u velocity, the highest frequency of interest is related to the smallest coherent scales between p_w and u . It was discussed in §§ 3.1 and 4.1 that only u -velocity scales at $\lambda_x/y \gtrsim 3$ are coherent with the wall pressure. For a start of the logarithmic region at $y^+ = 80$, this corresponds to scales of $\lambda_x^+ \leq 240$ and a frequency range below $f = \bar{U}_c/\lambda_x \approx 800$ Hz (convection velocity taken as the mean velocity at $y^+ = 80$). Hence, the frequencies of interest reside at frequencies on the left of the hatched region in figure 19(a,b). The gain and phase are relatively flat for this region, and hence, the Helmholtz correction has a minimal impact on the pressure fluctuations in this range. Nevertheless, the correction is still required for the validity of the wall-pressure spectrum at smaller scales. In this regard, the correction following (A7) can amplify high-frequency noise due to the fast decay of the gain beyond f_r . An application of a low-pass filter prevents this and was implemented following the literature (Tsuji *et al.* 2007; Gibeau & Ghaemi 2021) with a cutoff frequency of $f_v/u_\tau^2 = 0.25$ ($f = 3$ kHz). A spectrum of the Helmholtz-corrected pressure fluctuations p_{w3} is shown in figure 20(a) and shows the removal of the amplified energy near f_r .

Step 3: Remove facility noise. A final step involves the removal of any remaining facility noise with the aid of the free-stream acoustic measurement, $p_f(t)$. This measurement was achieved by mounting a microphone in the potential flow region. A GRAS RA0022 $\frac{1}{4}$ in. nosecone was installed to remove as much as possible the pressure fluctuations from the turbulence in the stagnation point (see photograph in figure 17c). The noise removal procedure was implemented according to the description in Gibeau & Ghaemi (2021) and is only briefly summarized here. A subtraction of an estimate of the facility noise, denoted as \hat{p}_f , from the wall-pressure signal at the inlet of the pinhole inlet, p_{w3} , is implemented following

$$p_{w4}(t) = p_{w3}(t) - \hat{p}_f(t). \quad (\text{A8})$$

The estimate of the facility noise does not equal the measured facility noise, p_f , given that the noise is measured at a different position (in the potential flow region). Moreover, even though a nosecone was installed, the measurement is still intrusive and can be subject to self-induced pressure fluctuations. To generate the estimate, the Wiener noise cancelling filter coefficients can be derived from the measurement data and be implemented through the convolution of a digital finite impulse response filter: $\hat{p}_f(t_d) = (c \circledast p_f)(t_d)$. To emphasize the discrete-time dependence, subscript ‘d’ is used. Filter coefficients $c(t_d)$ are defined for m time instants and they are obtained through the Wiener–Hopf equations, $\mathbf{R}c = r$, in which \mathbf{R} is a symmetric Toeplitz matrix of size $m \times m$ with the auto-correlations of p_f , and r is the two-point cross-correlation vector of p_{w3} and p_f and has size $m \times 1$. The unique solution $c = \mathbf{R}^{-1}r$ yields the filter coefficients. The filter step is implemented with an order of $m = 30 \times 10^3$ on the signals that were down-sampled by a factor of 5, thus leaving an effective sampling frequency of $f_s = 51.2/5 = 10.24$ kHz. A spectrum of the pressure fluctuations after the removal of the facility noise through (A8) is shown in figure 20(a) and highlights the removal of noise peaks that were still present in the p_{w3} signal. Finally, it was also attempted to directly remove all tunnel noise from only the centre pinhole-mounted microphone (without first performing step 1), however, that resulted in a noisier final spectrum.

The spectrum of p_{w4} is compared with the 1-D spatial spectrum of DNS in figure 20(b). Here frequency was transformed to wavelength using $\lambda_x = \bar{U}_c/f$ and a convection velocity

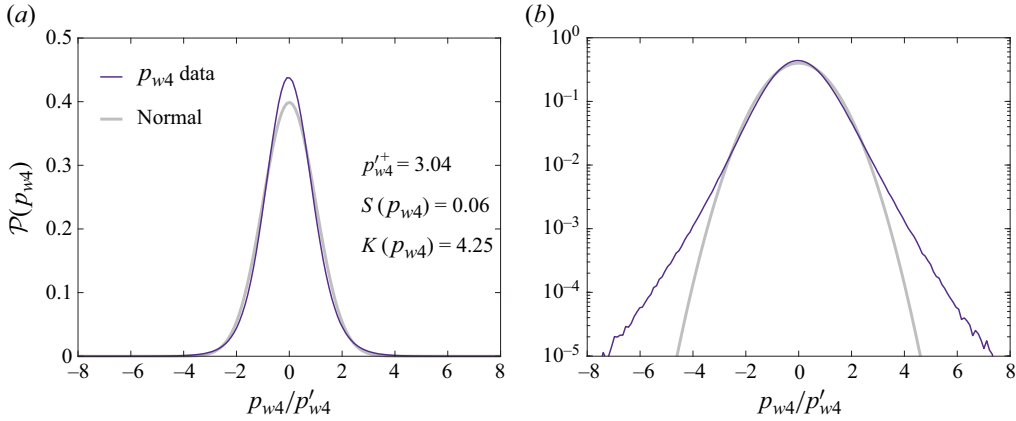


Figure 21. Probability density functions of the fluctuating wall-pressure signal, p_{w4} , with a (a) linear axis and (b) logarithmic axis. A normal PDF is shown for reference.

of $U_c^+ = 10$. In terms of integrated energy, the inner-scaled wall-pressure intensity from the experiments, $p'^+_{w4} \approx 3.04$, compares well with (A1) (Farabee & Casarella 1991; Klewicki *et al.* 2008) predicting a value of 3.31. The spectral density itself compares reasonably well at the mid-scale range. At the large-wavelength end of the spectrum the attenuation is expected due to the over-excessive removal of energy in step 1. At the small-wavelength end, the energy is amplified instead, presumably due to shortcomings in removing the Helmholtz resonance. That is, the transfer function in step 2 was generated using an acoustic calibration. However, a resonator behaves differently when excited by a grazing TBL flow, in comparison to an acoustic wave excitation, since the ‘end correction’ is changed and, thus, the resonance frequency and effective damping (Panton & Miller 1975). Nevertheless, the mismatch of the spectral shape does not affect any conclusions of the current work, given that the resonance is outside of the frequency range at which the scales of u and p_{w4} possess a non-zero coherence. Finally, comparing the experimental spectrum based on temporal data with the spatial DNS spectra is challenging. Frequency-to-wavenumber conversions are non-trivial and Taylor’s hypothesis can introduce aliasing-type discrepancies, particularly in the near-wall region (Perry & Li 1990; del Álamo & Jiménez 2009).

With the valid time series of the fluctuating wall pressure, p_{w4} , the PDF can be generated. Figure 21(a) shows the PDF with a linear ordinate and a normalization by the standard deviation. Around the zero-amplitude fluctuations, the PDF is larger than the associated normal distribution. In the tails of the PDF, being more evident with the semi-logarithmic axes in figure 21(b), a larger amplitude is also noticeable and the PDF tends more towards an exponential form. Similar PDF’s were shown in the literature (Tsuji *et al.* 2007; Klewicki *et al.* 2008). Tsuji *et al.* (2007) indicated that the skewness increased with the Reynolds number, from -0.05 to 0.09 for Re_θ ranging from 5870 to 16 700. Our skewness of 0.06 at $Re_\theta \approx 6190$ is slightly larger, but the exact skewness value is known to also depend on the value of d^+ (Schewe 1983; Gravante *et al.* 1998). Nevertheless, skewness values are small, and third-order moments in the QSE approach can therefore be neglected (Naguib *et al.* 2001).

REFERENCES

- ABBASSI, M.R., BAARS, W.J., HUTCHINS, N. & MARUSIC, I. 2017 Skin-friction drag reduction in a high-Reynolds-number turbulent boundary layer via real-time control of large-scale structures. *Intl J. Heat Fluid Flow* **67**, 30–41.
- ADRIAN, R.J. 1979 Conditional eddies in isotropic turbulence. *Phys. Fluids* **22** (11), 2065–2070.
- ADRIAN, R.J. & MOIN, P. 1988 Stochastic estimation of organized turbulent structure: homogeneous shear flow. *J. Fluid Mech.* **190**, 531–559.
- ADRIAN, R.J., MOIN, P. & MOSER, R.D. 1987 Stochastic estimation of conditional eddies in turbulent channel flow. *Proceedings of the Summer Program 1987, Center for Turbulence Research*, pp. 7–19, CTR-S87.
- DEL ÁLAMO, J.C. & JIMÉNEZ, J. 2003 Spectra of the very large anisotropic scales in turbulent channels. *Phys. Fluids* **15** (6), L41–L44.
- DEL ÁLAMO, J.C. & JIMÉNEZ, J. 2009 Estimation of turbulent convection velocities and corrections to Taylor's approximation. *J. Fluid Mech.* **640**, 5–26.
- ARUN, R., BAE, H.J. & MCKEON, B.J. 2023 Towards real-time reconstruction of velocity fluctuations in turbulent channel flow. *Phys. Rev. Fluids* **8**, 064612.
- BAARS, W.J., HUTCHINS, N. & MARUSIC, I. 2017 Self-similarity of wall-attached turbulence in boundary layers. *J. Fluid Mech.* **823**, R2.
- BAARS, W.J. & MARUSIC, I. 2020 Data-driven decomposition of the streamwise turbulence kinetic energy in boundary layers. Part 1. Energy spectra. *J. Fluid Mech.* **882**, A25.
- BAARS, W.J. & TINNEY, C.E. 2014 Proper orthogonal decomposition-based spectral higher-order stochastic estimation. *Phys. Fluids* **26**, 055112.
- BAI, H.L., ZHOU, Y., ZHANG, W.G., XU, S.J., WANG, Y. & ANTONIA, R.A. 2014 Active control of a turbulent boundary layer based on local surface perturbation. *J. Fluid Mech.* **750**, 316–354.
- BAIDYA, R., PHILIP, J., HUTCHINS, N., MONTY, J.P. & MARUSIC, I. 2017 Distance-from-the-wall scaling of turbulent motions in wall-bounded flows. *Phys. Fluids* **29**, 020712.
- CANTON, J., ÖRLU, R., CHIN, C. & SCHLATTER, P. 2016 Reynolds number dependence of large-scale friction control in turbulent channel flow. *Phys. Rev. Fluids* **1**, 081501.
- CHAUHAN, K.A., MONKEWITZ, P.A. & NAGIB, H.M. 2009 Criteria for assessing experiments in zero pressure gradient boundary layers. *Fluid Dyn. Res.* **41**, 021404.
- CHERNYSHENKO, S. 2021 Extension of QSQH theory of scale interaction in near-wall turbulence to all velocity components. *J. Fluid Mech.* **916**, A52.
- CHOI, H., MOIN, P. & KIM, J. 1994 Active turbulence control for drag reduction in wall-bounded flows. *J. Fluid Mech.* **262**, 75–110.
- CHOI, K.-S., DEBISSCHOP, J.-R. & CLAYTON, B.R. 1998 Turbulent boundary-layer control by means of spanwise-wall oscillation. *AIAA J.* **36** (7), 1157–1163.
- CHOI, K.-S., JUKES, T. & WHALLEY, R. 2011 Turbulent boundary-layer control with plasma actuators. *Phil. Trans. R. Soc. A* **369**, 1443–1458.
- CUI, G. & JACOBI, I. 2021 Biphasic as a diagnostic for scale interactions in wall-bounded turbulence. *Phys. Rev. Fluids* **6**, 014604.
- DACOME, G., MÖRSCH, R., KOTSONIS, M. & BAARS, W.J. 2023 Opposition flow control for reducing skin-friction drag of a turbulent boundary layer. [arXiv:2309.13929](https://arxiv.org/abs/2309.13929).
- DENG, B.Q., HUANG, W.X. & XU, C.X. 2016 Origin of effectiveness degradation in active drag reduction control of turbulent channel flow at $Re_\tau = 1000$. *J. Turbul.* **17** (8), 758–786.
- DESHPANDE, R., CHANDRAN, D., MONTY, J.P. & MARUSIC, I. 2020 Two-dimensional cross-spectrum of the streamwise velocity in turbulent boundary layers. *J. Fluid Mech.* **890**, R2.
- EWING, D. & CITRINITI, J. 1999 Examination of a LSE/POD complementary technique using single and multi-time information in the axisymmetric shear layer. In *Proceedings of the IUTAM Symposium on Simulation and Identification of Organized Structures in Flows* (ed. J.N. Sorensen, E.J. Hopfinger & N. Aubry), pp. 375–384. IUTAM.
- FARABEE, T.M. & CASARELLA, M.J. 1991 Spectral features of wall pressure fluctuations beneath turbulent boundary layers. *Phys. Fluids A* **3** (10), 2410–2420.
- GHAEMI, S. & SCARANO, F. 2013 Turbulent structure of high-amplitude pressure peaks within the turbulent boundary layer. *J. Fluid Mech.* **735**, 381–426.
- GIBEAU, B. & GHAEMI, S. 2021 Low- and mid-frequency wall-pressure sources in a turbulent boundary layer. *J. Fluid Mech.* **918**, A18.
- GRAVANTE, S.P., NAGUIB, A.M., WARK, C.E. & NAGIB, H.M. 1998 Characterization of the pressure fluctuations under a fully developed turbulent boundary layer. *AIAA J.* **36** (10), 1808–1816.

- GUASTONI, L., GÜMES, A., IANIRO, A., DISCETTI, S., SCHLATTER, P., AZIZPOUR, H. & VINUESA, R. 2021 Convolutional-network models to predict wall-bounded turbulence from wall quantities. *J. Fluid Mech.* **928**, A27.
- GUEZENNEC, Y.G. 1989 Stochastic estimation of coherent structures in turbulent boundary layers. *Phys. Fluids A* **1** (6), 1054–1060.
- HAMILTON, J.M., KIM, J. & WALEFFE, F. 1995 Regeneration mechanisms of near-wall turbulence structures. *J. Fluid Mech.* **287**, 317–348.
- HULTMARK, M. & SMITS, A.J. 2010 Temperature corrections for constant temperature and constant current hot-wire anemometers. *Meas. Sci. Technol.* **21**, 105404.
- HUTCHINS, N., MONTY, J.P., GANAPATHISUBRAMANI, B., NG, H.C.H. & MARUSIC, I. 2011 Three-dimensional conditional structure of a high Reynolds number turbulent boundary layer. *J. Fluid Mech.* **673**, 255–285.
- HUTCHINS, N., NICKELS, T.B., MARUSIC, I. & CHONG, M.S. 2009 Hot-wire spatial resolution issues in wall-bounded turbulence. *J. Fluid Mech.* **635**, 103–136.
- HWANG, Y.F., BONNESS, W.K. & HAMBRIC, S.A. 2009 Comparison of semi-empirical models for turbulent boundary layer wall pressure spectra. *J. Sound Vib.* **319**, 199–217.
- INGARD, U. 1953 On the theory and design of acoustic resonators. *J. Acoust. Soc. Am.* **25** (6), 1037–1061.
- JIMÉNEZ, J. & HOYAS, S. 2008 Turbulent fluctuations above the buffer layer of wall-bounded flows. *J. Fluid Mech.* **611**, 215–236.
- KASAGI, N., SUZUKI, Y. & FUKAGATA, K. 2009 Microelectromechanical systems-based feedback control of turbulence for skin friction reduction. *Annu. Rev. Fluid Mech.* **41**, 231–251.
- KLEWICKI, J.C., PRIYADARSHANA, P.J.A. & METZGER, M.M. 2008 Statistical structure of the fluctuating wall pressure and its in-plane gradients at high Reynolds number. *J. Fluid Mech.* **609**, 195–220.
- LASAGNA, D., ORAZI, M. & IUSO, G. 2013 Multi-time delay, multi-point linear stochastic estimation of a cavity shear layer velocity from wall-pressure measurements. *Phys. Fluids* **25**, 017101.
- LEE, C., KIM, J. & CHOI, H. 1998 Suboptimal control of turbulent channel flow for drag reduction. *J. Fluid Mech.* **358**, 245–258.
- LEE, M. & MOSER, R.D. 2015 Direct numerical simulation of turbulent channel flow up to $Re_\tau = 5200$. *J. Fluid Mech.* **774**, 395–415.
- LEE, M. & MOSER, R.D. 2019 Spectral analysis of the budget equation in turbulent channel flows at high Reynolds number. *J. Fluid Mech.* **860**, 886–938.
- LIU, C. & GAYME, D.F. 2020 An input–output based analysis of convective velocity in turbulent channels. *J. Fluid Mech.* **888**, A32.
- MADHUSUDANAN, A., ILLINGWORTH, S.J. & MARUSIC, I. 2019 Coherent large-scale structures from the linearized Navier–Stokes equations. *J. Fluid Mech.* **873**, 89–109.
- MATHIS, R., HUTCHINS, N. & MARUSIC, I. 2009 Large-scale amplitude modulation of the small-scale structures in turbulent boundary layers. *J. Fluid Mech.* **628**, 311–337.
- MERINO-MARTÍNEZ, R., CARPIO, A.R., PEREIRA, L.L., VAN HERK, S., AVALLONE, F., RAGNI, D. & KOTSONIS, M. 2020 Aeroacoustic design and characterization of the 3D-printed, open-jet, anechoic wind tunnel of Delft University of Technology. *Appl. Acoust.* **170**, 107504.
- MURRAY, N.E. & UKEILEY, L.S. 2003 Estimation of the flowfield from surface pressure measurements in an open cavity. *AIAA J.* **41** (5), 969–972.
- MURRAY, N.E. & UKEILEY, L.S. 2004 Low-dimensional estimation of cavity flow dynamics. In *AIAA Paper 2004-681*.
- NAGUIB, A.M., GRAVANTE, S.P. & WARK, C.E. 1996 Extraction of turbulent wall-pressure time-series using an optimal filtering scheme. *Exp. Fluids* **22**, 14–22.
- NAGUIB, A.M., WARK, C.E. & JUCKENHÖFEL, O. 2001 Stochastic estimation and flow sources associated with surface pressure events in a turbulent boundary layer. *Phys. Fluids* **13** (9), 2611–2626.
- NAKA, Y., STANISLAS, M., FOUCAUT, J.-M., COUDERT, S., LAVAL, J.-P. & OBI, S. 2015 Space–time pressure–velocity correlations in a turbulent boundary layer. *J. Fluid Mech.* **771**, 624–675.
- ORSZAG, S.A. 1971 On the elimination of aliasing in finite-difference schemes by filtering high-wavenumber components. *J. Atmos. Sci.* **28** (6), 1074–1074.
- PANTON, R.L., LEE, M. & MOSER, R.D. 2017 Correlation of pressure fluctuations in turbulent wall layers. *Phys. Rev. Fluids* **2**, 094604.
- PANTON, R.L. & MILLER, J.M. 1975 Resonant frequencies of cylindrical Helmholtz resonators. *J. Acoust. Soc. Am.* **57** (6), 1533–1535.
- PERRY, A.E. & LI, J.D. 1990 Experimental support for the attached-eddy hypothesis in zero-pressure-gradient turbulent boundary layers. *J. Fluid Mech.* **218**, 405–438.

- QIAO, Z.X., WU, Z. & ZHOU, Y. 2018 Turbulent boundary layer manipulation under a proportional-derivative closed-loop scheme. *Phys. Fluids* **30**, 115101.
- RATHNASINGHAM, R. & BREUER, K.S. 2003 Active control of turbulent boundary layers. *J. Fluid Mech.* **495**, 209–233.
- RENARD, N. & DECK, S. 2016 A theoretical decomposition of mean skin friction generation into physical phenomena across the boundary layer. *J. Fluid Mech.* **790**, 339–367.
- SCHWEWE, G. 1983 On the structure and resolution of wall-pressure fluctuations associated with turbulent boundary-layer flow. *J. Fluid Mech.* **134**, 311–328.
- SCHOPPA, W. & HUSSAIN, F. 1998 A large-scale control strategy for drag reduction in turbulent boundary layers. *Phys. Fluids* **10** (5), 1049–1051.
- SCHULTZ, M.P. & FLACK, K.A. 2007 The rough-wall turbulent boundary layer from the hydraulically smooth to the fully rough regime. *J. Fluid Mech.* **580**, 381–405.
- SMITS, A.J., HULTMARK, M., LEE, M. & PIROZZOLI, S. 2021 Reynolds stress scaling in the near-wall region of wall-bounded flows. *J. Fluid Mech.* **926**, A31.
- SMITS, A.J., MCKEON, B.J. & MARUSIC, I. 2011a High Reynolds number wall turbulence. *Annu. Rev. Fluid Mech.* **43**, 353–375.
- SMITS, A.J., MONTY, J., HULTMARK, M., BAILEY, S.C.C., HUTCHINS, N. & MARUSIC, I. 2011b Spatial resolution correction for wall-bounded turbulence measurements. *J. Fluid Mech.* **676**, 41–53.
- THOMAS, A.S.W. & BULL, M.K. 1983 On the role of wall-pressure fluctuations in deterministic motions in the turbulent boundary layer. *J. Fluid Mech.* **128**, 283–322.
- TINNEY, C.E., COIFFET, F., DELVILLE, J., GLAUSER, M.N., JORDAN, P. & HALL, A.M. 2006 On spectral linear stochastic estimation. *Exp. Fluids* **41** (5), 763–775.
- TSUJI, Y., FRANSSON, J.H.M., ALFREDSSON, P.H. & JOHANSSON, A.V. 2007 Pressure statistics and their scaling in high-Reynolds-number turbulent boundary layers. *J. Fluid Mech.* **585**, 1–40.
- VAN BLITTERSWYK, J. & ROCHA, J. 2017 An experimental study of the wall-pressure fluctuations beneath low Reynolds number turbulent boundary layers. *J. Acoust. Soc. Am.* **141** (2), 1257–1268.
- WILLMARTH, W.W. 1975 Pressure fluctuations beneath turbulent boundary layers. *Annu. Rev. Fluid Mech.* **7**, 13–36.
- YAO, J., CHEN, X. & HUSSAIN, F. 2018 Drag control in wall-bounded turbulent flows via spanwise opposed wall-jet forcing. *J. Fluid Mech.* **852**, 678–709.
- ZHANG, C. & CHERNYSHENKO, S.I. 2016 Quasisteady quasihomogeneous description of the scale interactions in near-wall turbulence. *Phys. Rev. Fluids* **1**, 014401.